

05

Advance Analysis

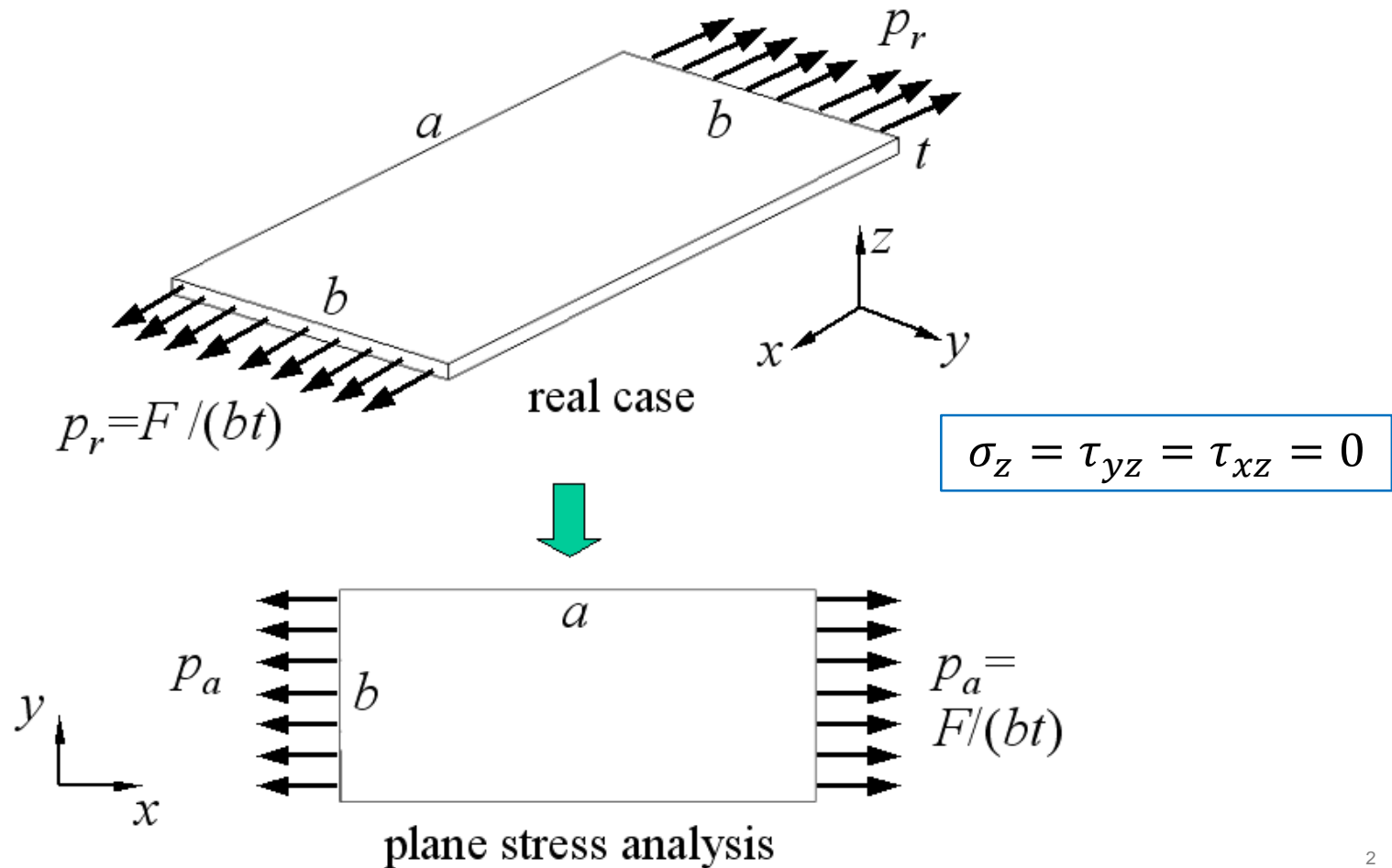
多步驟分析 / 平面應變&平面應力
非線性分析(接觸&材料設定) / 結構最佳化



2D Plane Problem



- Plane stress, plane strain, axisymmetric, plane stress w/thk
- Plane stress

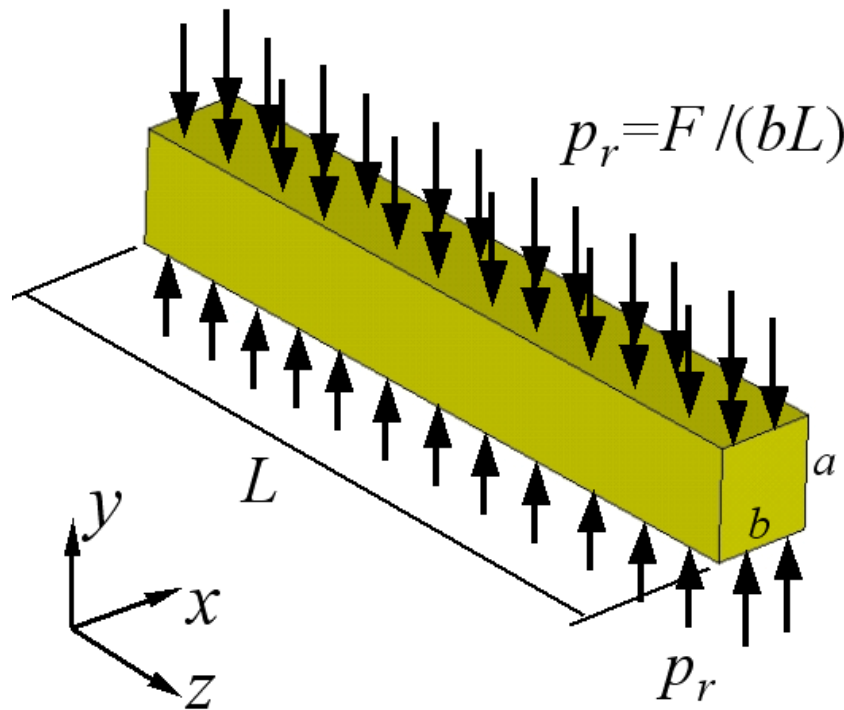


2D Plane Problem

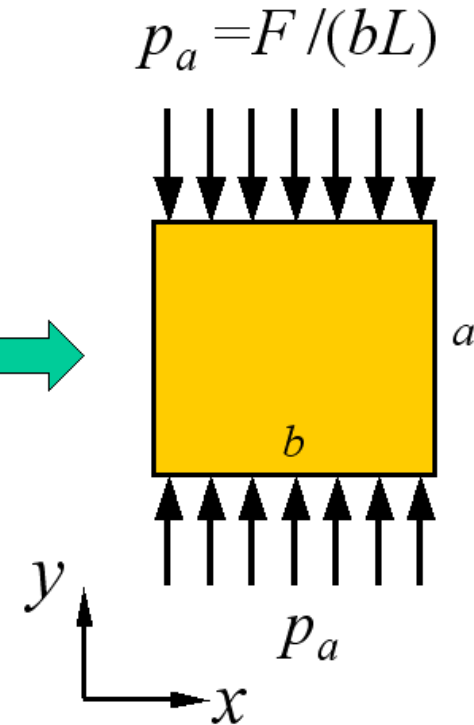
■ Plane strain

- The cross-sections are along the thickness

$$\varepsilon_z = \gamma_{yz} = \gamma_{xz} = 0$$



real case



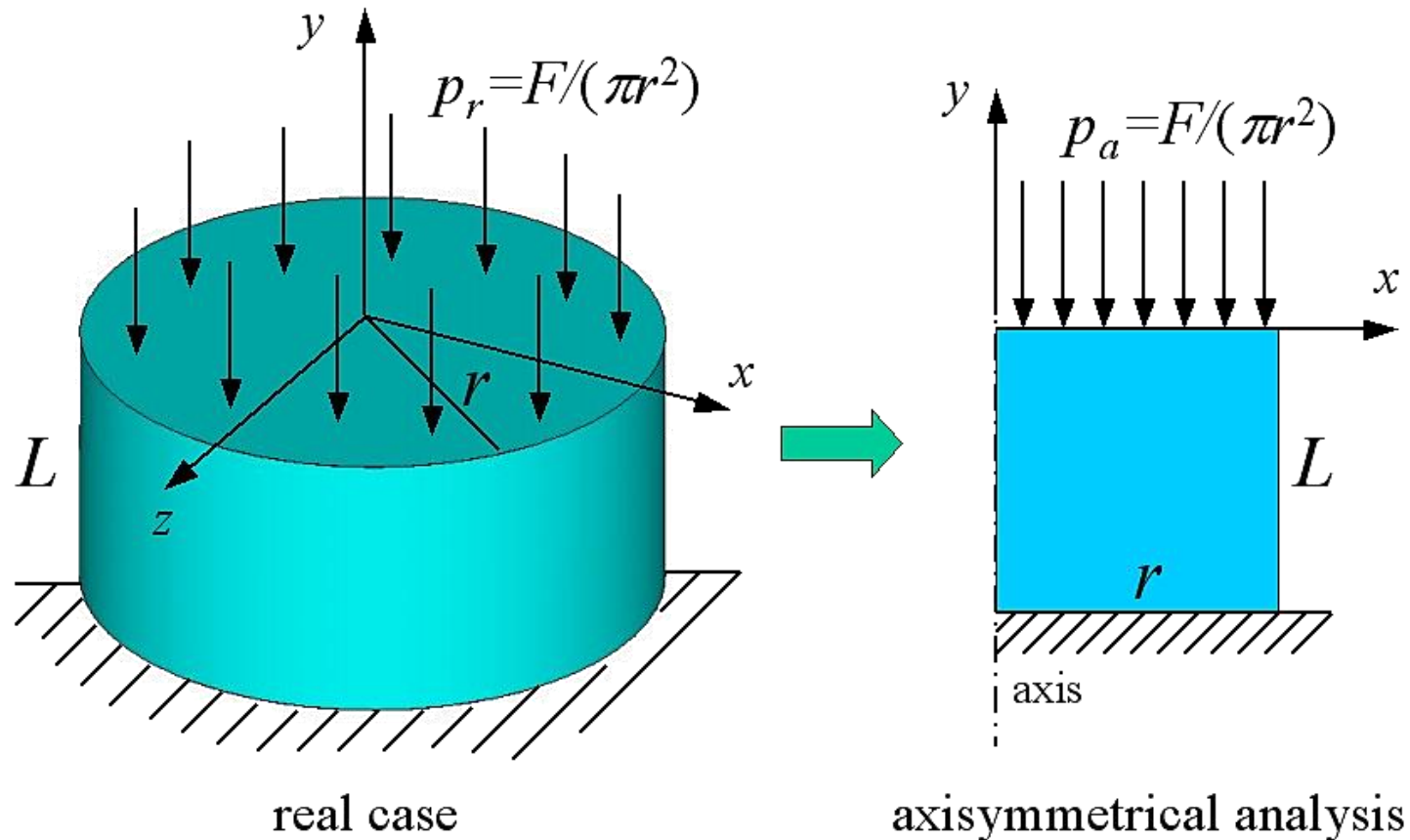
plane strain analysis



2D Plane Problem

■ Axisymmetric

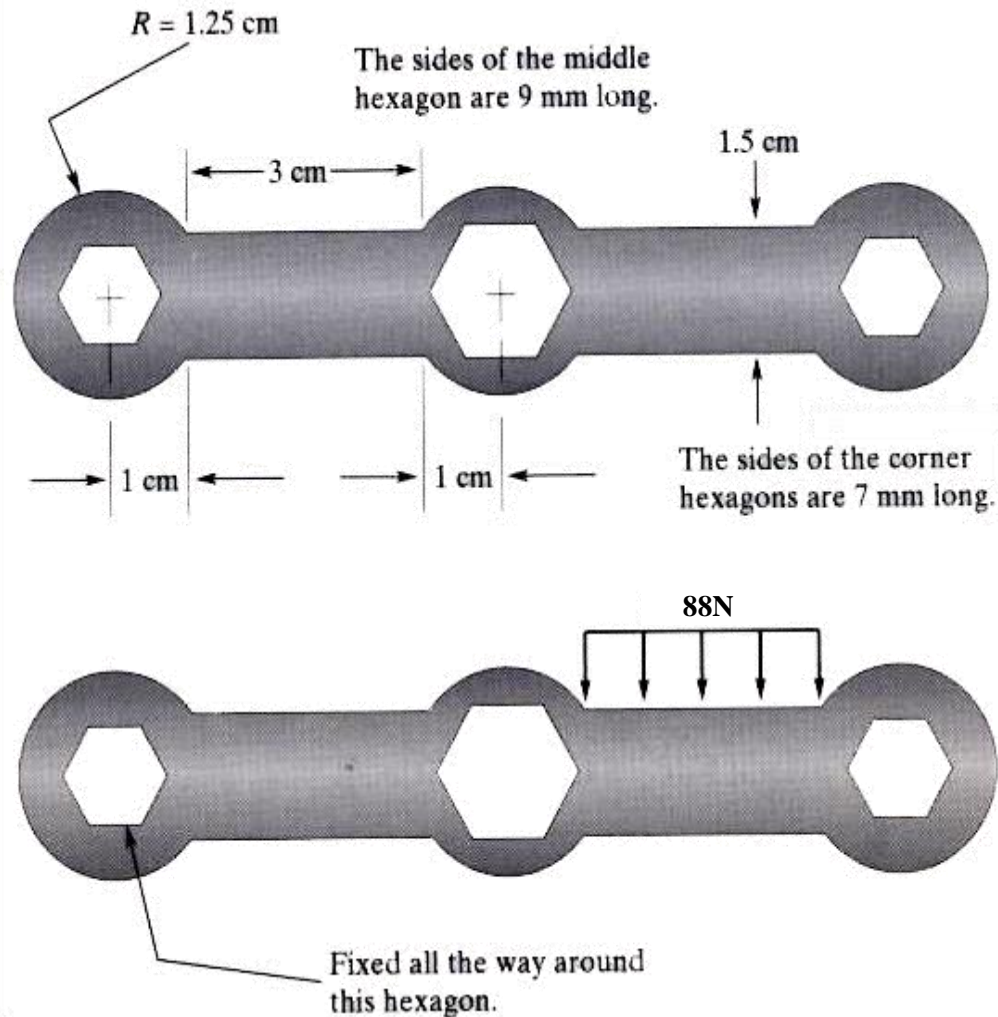
- The cross-sections are along the radial directions



Plane Stress – Ex.10



The bicycle wrench shown in figure is made of steel with 3 mm thick. Determine the von-Mises stresses under the given distributed load and boundary conditions.

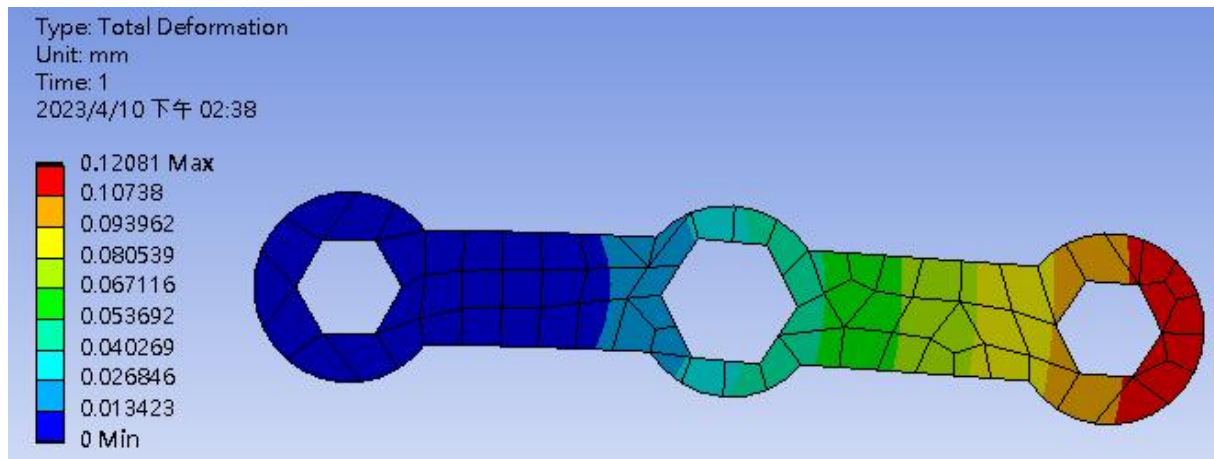


Plane Stress – Ex.10

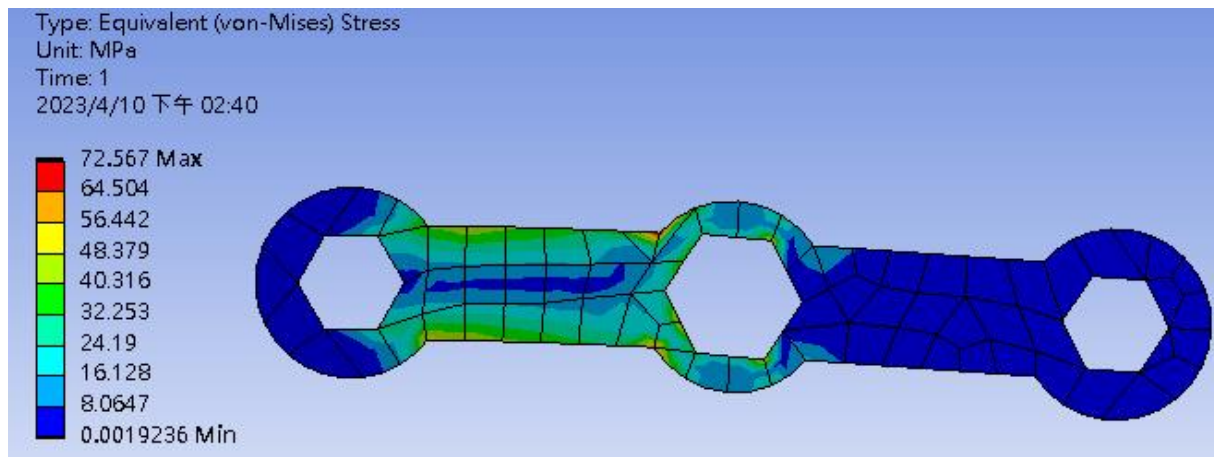
學習目標

- 2D分析設定
- 單位轉換
- Polygon

The bicycle wrench shown in figure is made of steel with 3 mm thick. Determine the von-Mises stresses under the given distributed load and boundary conditions.



變形量
Total Deformation



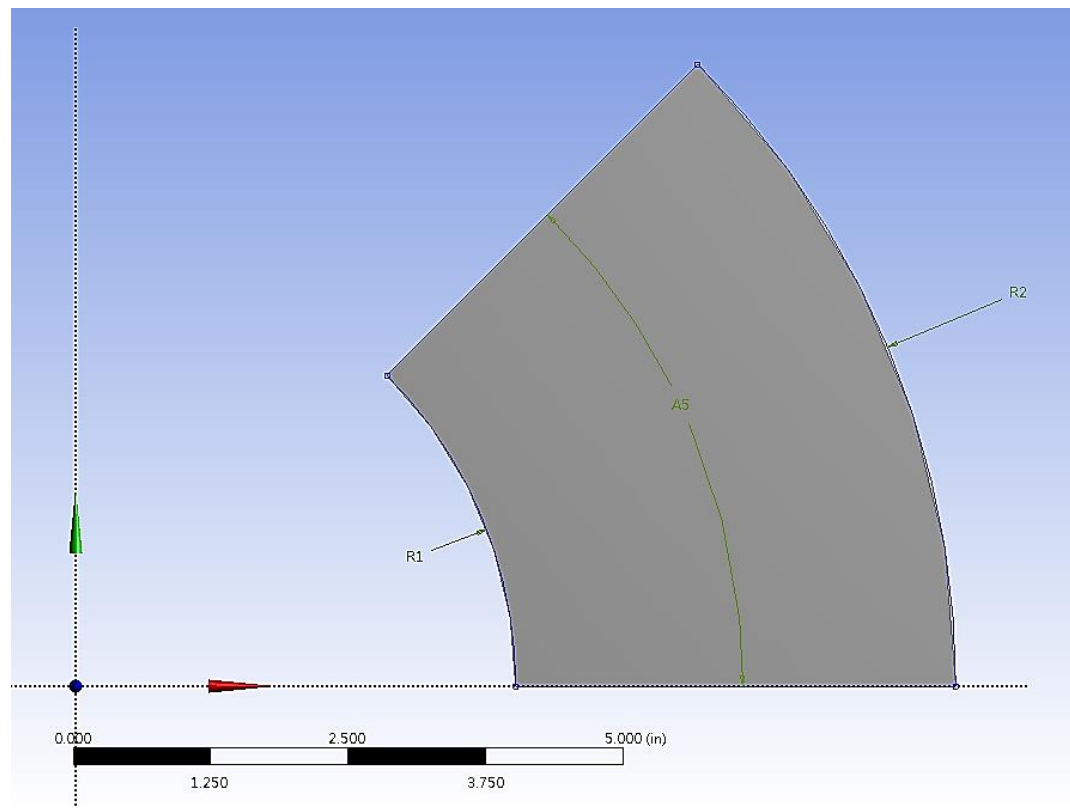
等效應力
Equivalent Stress

Plane Strain – Ex.11



Stresses in a Long Cylinder

A long thick-walled cylinder (with inner radius = 4 in. and outer radius = 8 in.) made of steel is initially subjected to an constant pressure (of 30000 psi). The pressure is then removed and the cylinder is subjected to a constant rotation (60000 rpm) about its center line. Find the radial displacement, radial stress, and hoop stress at the two load steps. (Face mesh size = 0.25 in)



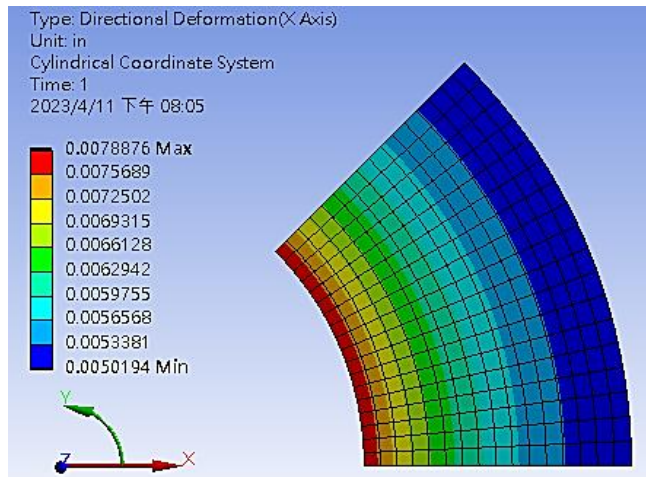
Plane Strain – Ex.11-1

- 學習目標
- 圓柱座標轉換
 - *Face Meshing*
 - 角速度設定
 - 多步驟分析

Stresses in a Long Cylinder

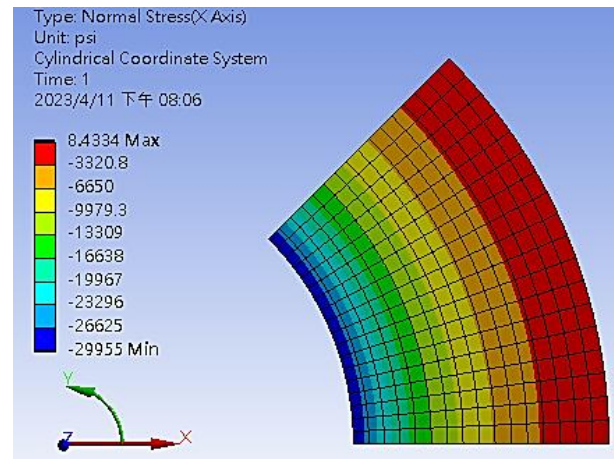
A long thick-walled cylinder (with inner radius = 4 in. and outer radius = 8 in.) made of steel is initially subjected to an constant pressure (of 30000 psi). The pressure is then removed and the cylinder is subjected to a constant rotation (60000 rpm) about its center line. Find the radial displacement, radial stress, and hoop stress at the two load steps. (Face mesh size = 0.25 in)

Step. 1



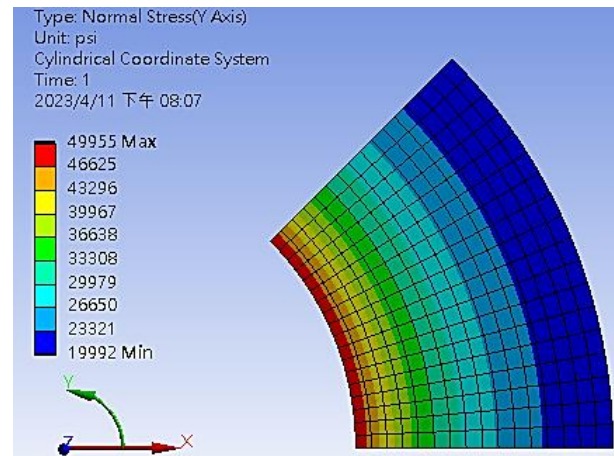
Directional Deformation

Radial displacement



Normal stress

Radial stress



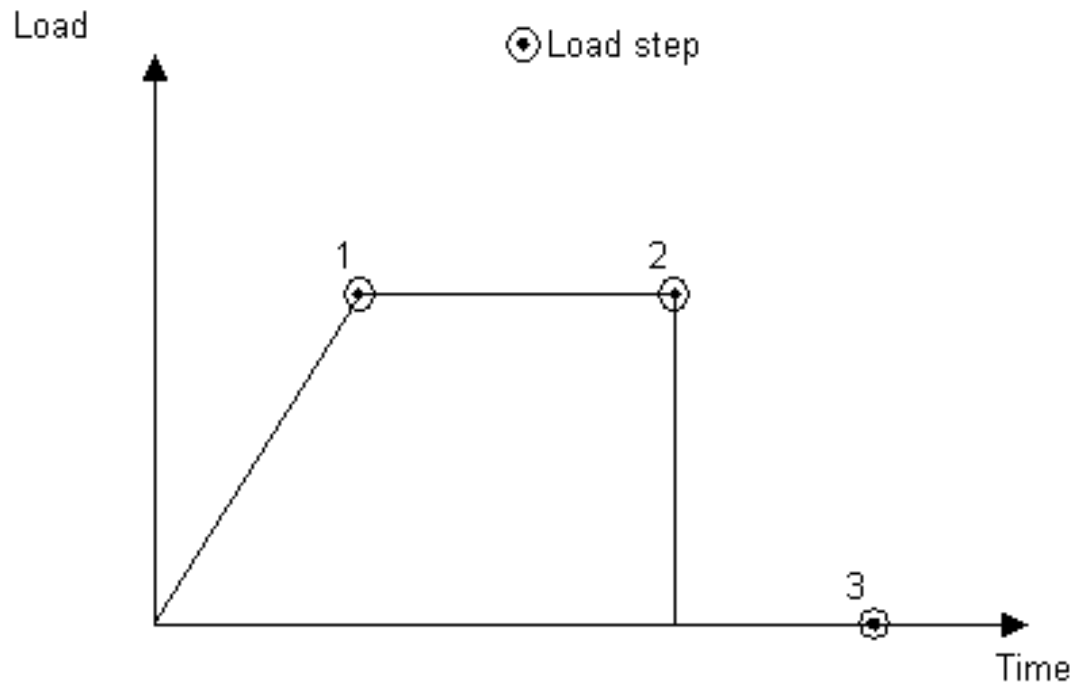
Normal stress

Hook stress



■ Load Steps

- In a linear static or steady-state analysis, you can use different load steps to apply different sets of loads--wind load in the first load step, gravity load in the second load step, both loads and a different support condition in the third load step, and so on.
- In a transient analysis, multiple load steps apply different segments of the load history curve.

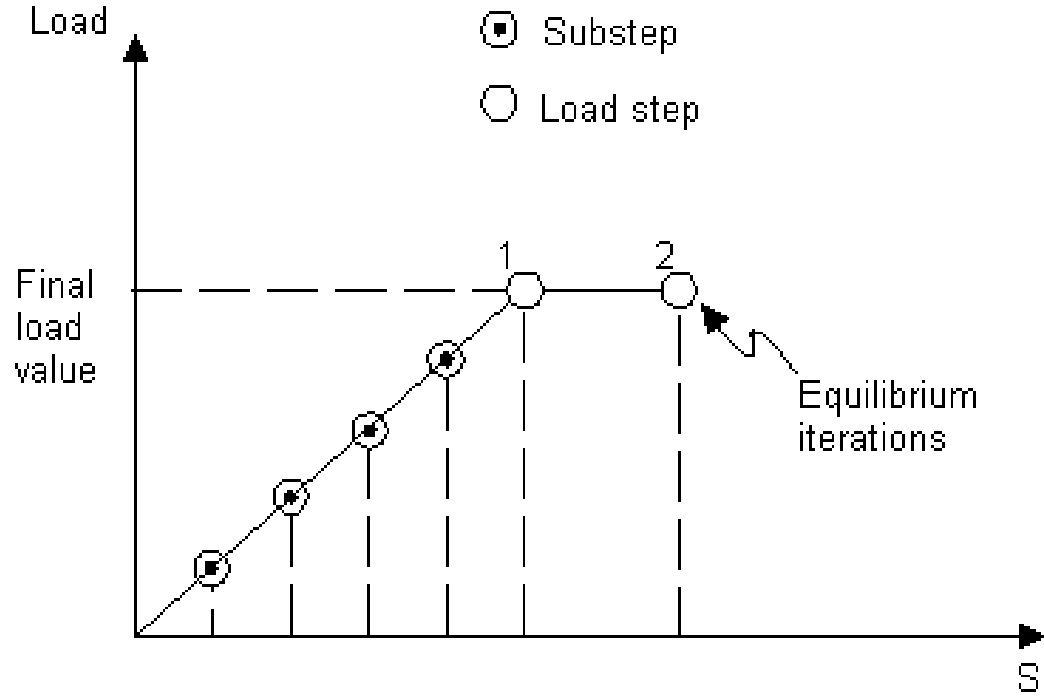


Introduction of ANSYS – Solution



■ Substeps

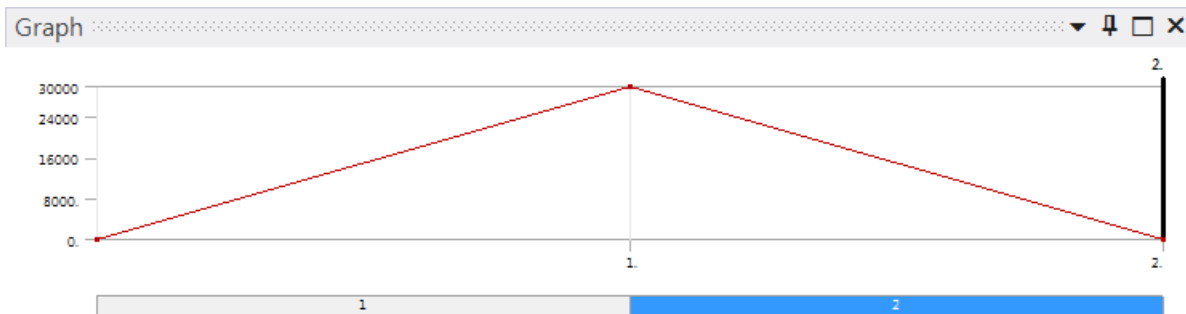
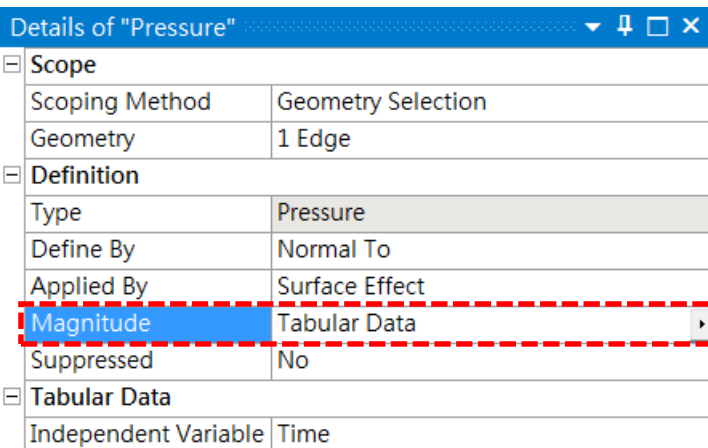
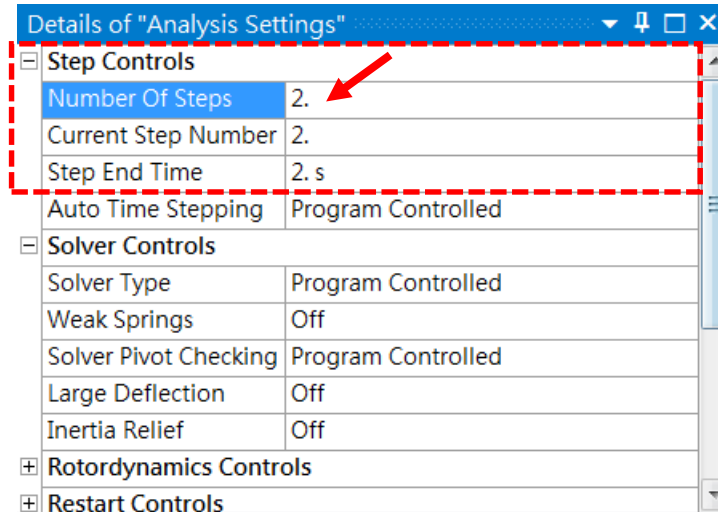
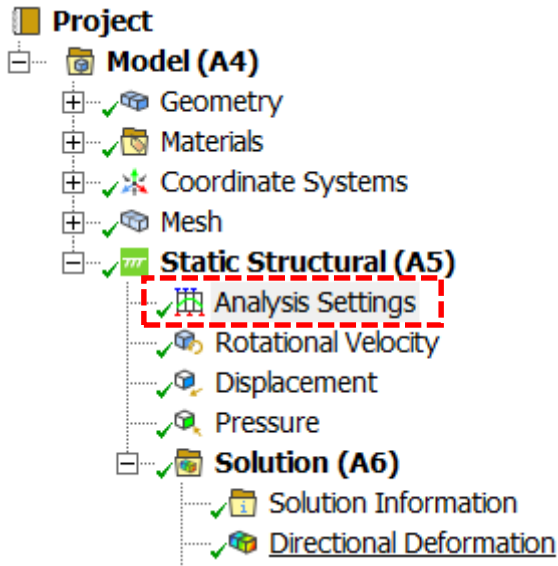
- **Substeps are points within a load step at which solutions are calculated. You use them for different reasons:**
 - ✓ In a linear or nonlinear transient analysis, use substeps to satisfy transient time integration rules
 - ✓ In a nonlinear static or steady-state analysis, use substeps to apply the loads gradually so that an accurate solution can be obtained.



Introduction of ANSYS – Solution



■ Step Controls



| Tabular Data | | | |
|--------------|-------|----------|----------------|
| | Steps | Time [s] | Pressure [psi] |
| 1 | 1 | 0. | 0. |
| 2 | 1 | 1. | 30000 |
| 3 | 2 | 2. | 0. |
| * | | | |

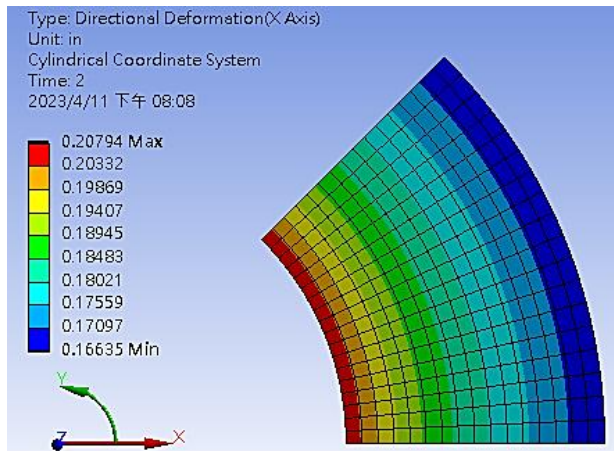
Plane Strain – Ex.11-2

- 學習目標
- 圓柱座標轉換
 - *Face Meshing*
 - 角速度設定
 - 多步驟分析

Stresses in a Long Cylinder

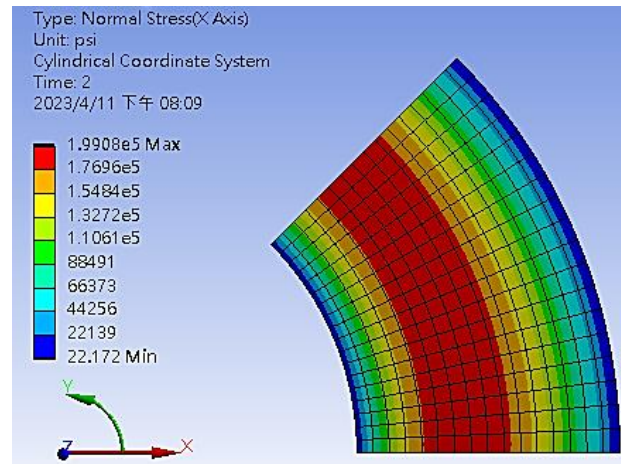
A long thick-walled cylinder (with inner radius = 4 in. and outer radius = 8 in.) made of steel is initially subjected to an constant pressure (of 30000 psi). The pressure is then removed and the cylinder is subjected to a constant rotation (60000 rpm) about its center line. Find the radial displacement, radial stress, and hoop stress at the two load steps. (Face mesh size = 0.25 in)

Step. 2



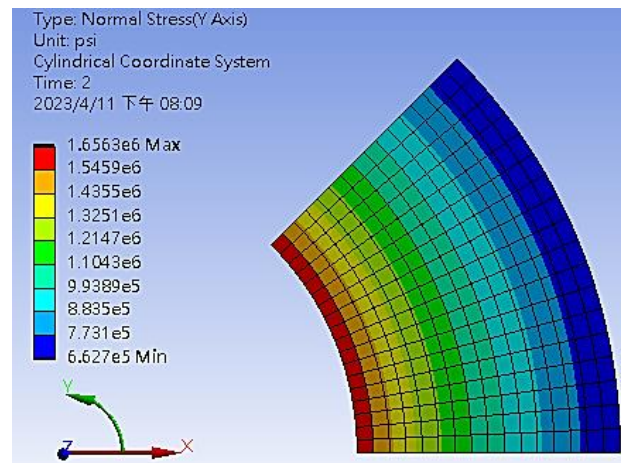
Directional Deformation

Radial displacement



Normal stress

Radial stress



Normal stress

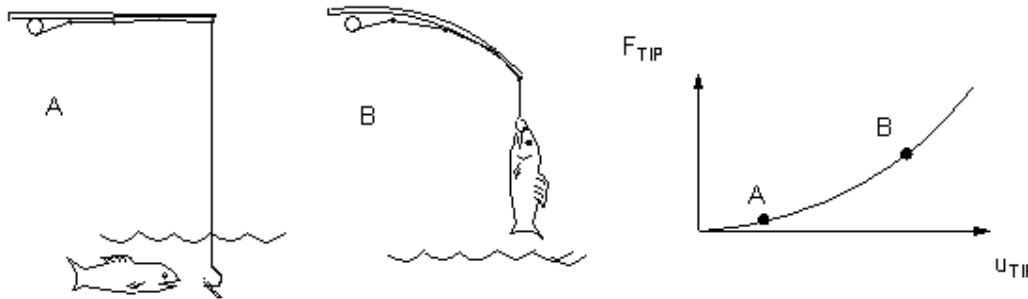
Hook stress

Nonlinear Structural Analysis

■ 有限元素法中，常見的非線性(Nonlinear)問題主要可分為三類

➤ 幾何非線性(Geometric nonlinearity)

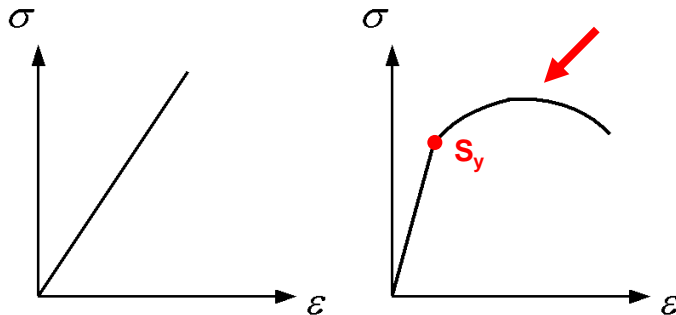
✓ 大變形、大位移



幾何非線性分析需開啟 **Large Deflection**，當節點位置產生變化，將重新計算其剛度矩陣

➤ 材料非線性(Material nonlinearity)

✓ 非線性行為之材料特性，即應力應變曲線非線性關係



設定 **Engineering Data**，指定為非線性材料性質

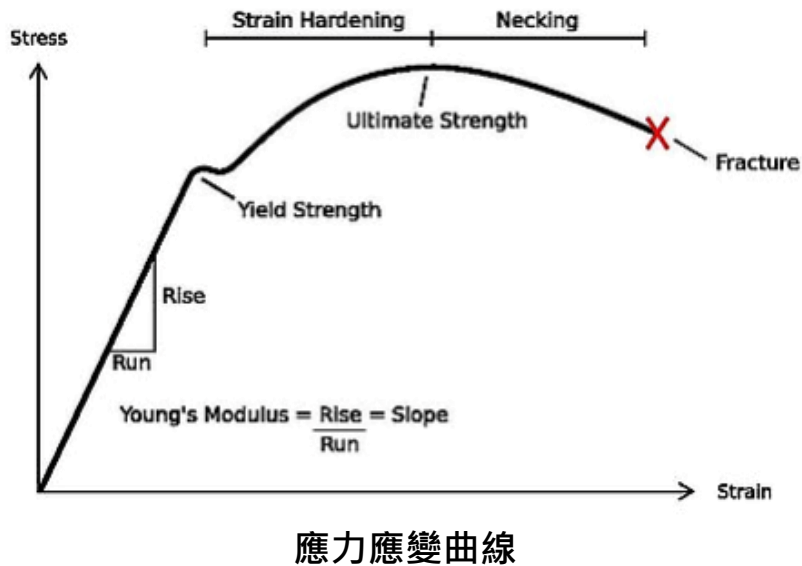
➤ 邊界非線性(Contact analysis)

✓ 非線性之接觸行為，如: **Frictional**、**Frictionless**、**Rough**



Material Nonlinearity

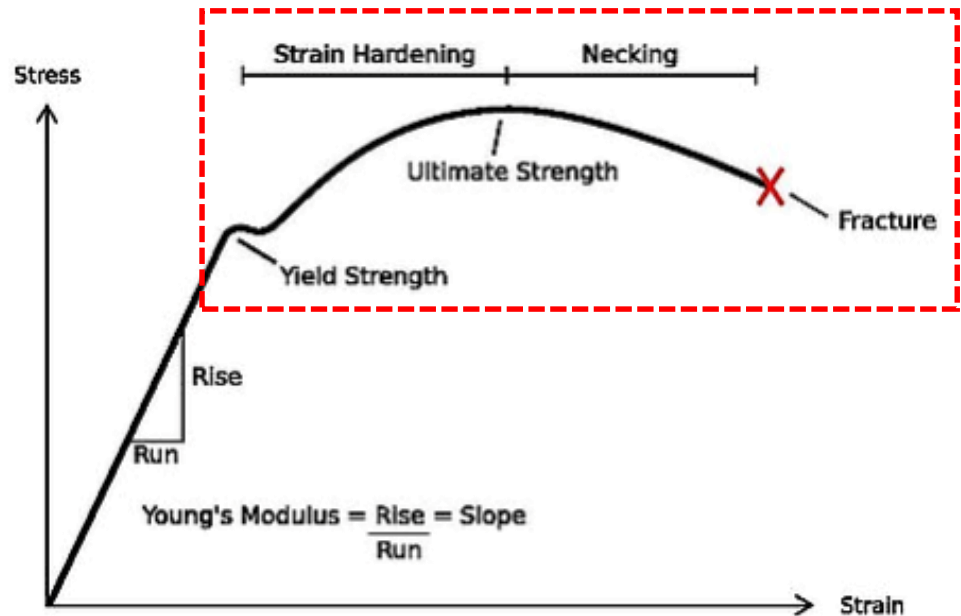
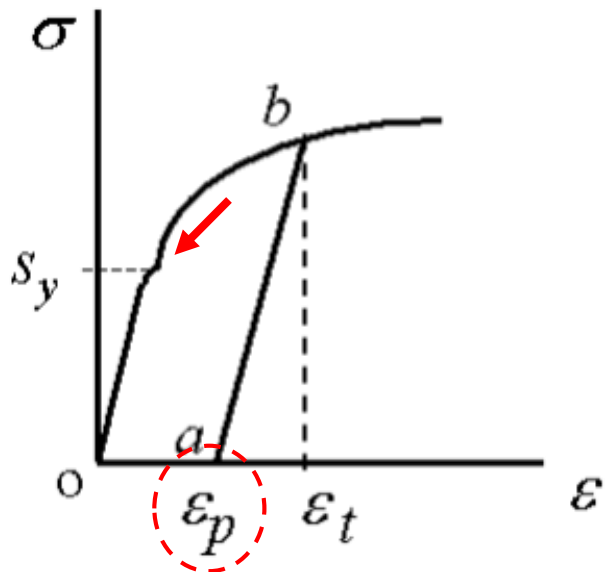
- 若應力分析範圍大於降伏強度，因應力與應變呈曲線關係，便成為材料非線性分析，這和遵循虎克定律之線彈性分析完全不同
- 在結構分析中，若負荷過程的應力包含了彈性部分與超過強伏點的塑性部分，可稱為彈塑性(elastoplastic)分析



| 材料行為 | 變形型式 | 與應變率(或時間)之關係 (Rate dependency) | 材料性質分類 | 材料模型 (Material laws) |
|------|------|--------------------------------|---|------------------------------------|
| 線性 | 彈性 | 無關 (Rate-independent) | Linear elastic | Hooke's law |
| 非線性 | 彈性 | 無關 (Rate-independent) | Hyperelastic | Mooney-Rivlin |
| | | | | Arruda-Boyce |
| | | | | Blatz-Ko |
| | | | Multilinear elastic | Multilinear elastic |
| | | 相關 (Rate-dependent) | Viscoelasticity | Viscoelasticity |
| | 非彈性 | 無關 (Rate-independent) | Isotropic hardening plasticity | Bilinear isotropic |
| | | | | Multilinear isotropic |
| | | | | Voce's nonlinear isotropic |
| | | | | Anisotropic |
| | | | Kinematic hardening plasticity | Bilinear kinematic |
| | | | | Multilinear kinematic |
| | | 相關 (Rate-dependent) | Combined kinematic and isotropic hardening plasticity | Chaboche |
| | | | | Chaboche and bilinear isotropic |
| | | | | Chaboche and multilinear isotropic |
| | | | | Chaboche and Voce's |
| | | | Pressure-dependent plasticity | Druger-Prager |
| | | | Viscoplasticity | Creep |
| | | | | Anand |
| | | | | Creep and bilinear isotropic |
| | | | | Creep and multilinear isotropic |
| | | | Combined creep and isotropic hardening plasticity | Creep and Voce's |

Material Nonlinearity – 彈塑性分析

- 塑性力學(plasticity)所研究的對象是延性材料在降伏後(應力 $> s_y$)所發生的塑性變形，屬於材料非線性分析的一種，由圖可看出結構受力過程包括了彈性與塑性變形，這類分析稱為彈塑性(elastoplastic)分析
- 材料達到塑性後，主要現象為產生應變硬化(strain hardening)與永久變形
- 若材料達到塑性變形(應力 $> s_y$)，當外力移除後將留下永久變形，圖中之 ϵ_p 即為移除外力後所殘留之塑性應變(plastic strain)，且在許多情況下會有殘留應力(residual stress)存在於材料內部

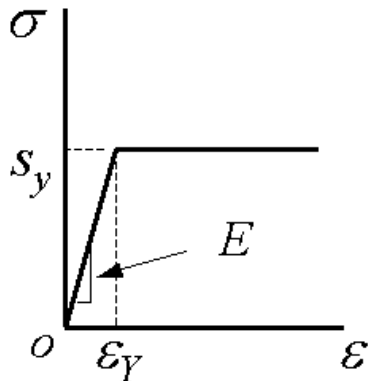




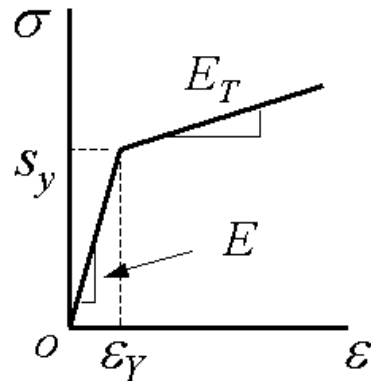
Material Nonlinearity – 彈塑性分析

■ 相對的在數學解析或有限元素分析上，有以下幾種應力應變曲線模式：

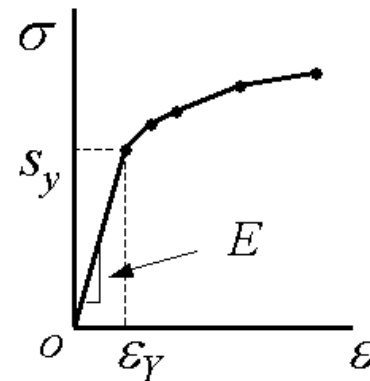
1. 彈性-完全塑性(elastic perfectly-plastic)
2. 雙線性(bi-linear)
3. 多線段(multi-linear)
4. 塑性曲線



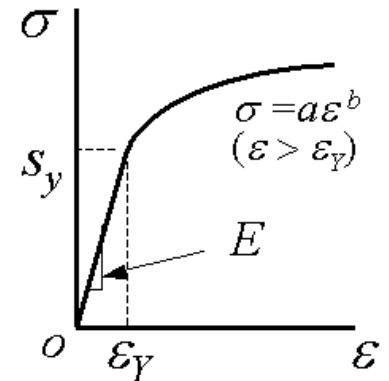
彈性-完全塑性



雙線性



多線段



塑性曲線

Introduction of ANSYS Workbench

■ Engineering Data(工程資料)

| | |
|---|--------------------|
| ▼ | A |
| 1 | Static Structural |
| 2 | Engineering Data ✓ |
| 3 | DM Geometry ✓ |
| 4 | Model ✓ |
| 5 | Setup ? |
| 6 | Solution ⚡ |
| 7 | Results ⚡ |

Unsaved Project - Workbench

File View Tools Units Help

New Open... Save Save As... Import... Reconnect Refresh Project Update Project Return to Project Compact Mode

Toolbox

- Physical Properties
 - Linear Elastic
 - Isotropic Elasticity
 - Orthotropic Elasticity
 - Anisotropic Elasticity
 - Experimental Stress Strain Data
 - Uniaxial Test Data
 - Biaxial Test Data
 - Shear Test Data
 - Volumetric Test Data
 - Simple Shear Test Data
 - Uniaxial Tension Test Data
 - Uniaxial Compression Test Data
 - Hyperelastic
 - Neo-Hookean
 - Arruda-Boyce
 - Gent
 - Blatz-Ko
 - Mooney-Rivlin 2 Parameter
 - Mooney-Rivlin 3 Parameter
 - Mooney-Rivlin 5 Parameter
 - Mooney-Rivlin 9 Parameter
 - Polynomial 1st Order
 - Polynomial 2nd Order
 - Polynomial 3rd Order

Outline of Schematic A2: Engineering Data

| | A | B | C | D |
|---|----------------------------------|---|---|---|
| 1 | Contents of Engineering Data | | | Description |
| 2 | Material | | | |
| 3 | Structural Steel | | | Fatigue Data at zero mean stress comes from 1998 ASME BPV Code, Section 8, Div 2, Table 5-110.1 |
| 4 | cortical bone | | | |
| * | Click here to add a new material | | | |

材料號碼及名稱

Properties of Outline Row 4: cortical bone

| | A | B | C | D | E |
|---|----------------------|--------------|------|---|---|
| 1 | Property | Value | Unit | | |
| 2 | Isotropic Elasticity | | | | |
| 3 | Derive from | Young's M... | | | |
| 4 | Young's Modulus | 17000 | MPa | | |
| 5 | Poisson's Ratio | 0.3 | | | |
| 6 | Bulk Modulus | 1.4167E | | | |
| 7 | Shear Modulus | 6.5385E | | | |

數值輸入

Table of Properties Row 5: Isotropic Elasticity

| | A | B |
|---|-----------------|-----------------|
| 1 | Temperature (C) | Poisson's Ratio |
| 2 | | 0.3 |
| * | | |

Chart of Properties Row 5: Isotropic Elasticity

Poisson's Ratio

Temperature [C]

材料特性種類

Messages

| | A | B | C | D |
|---|--------|---|-------------|-----------|
| 1 | Type | Text | Association | Date/Time |
| 2 | Events | Automotive Powertrain Fluid-Structure Interaction (FSI) | | |
| 3 | Events | Ask the Expert - External Data Mapping in ANSYS Workbench & Mechanical 14.0 | | |
| 4 | Events | Understanding Hardware Selection for Structural Mechanics | | |
| 5 | Events | SPE Annual Technical Conference & Exhibition | | |

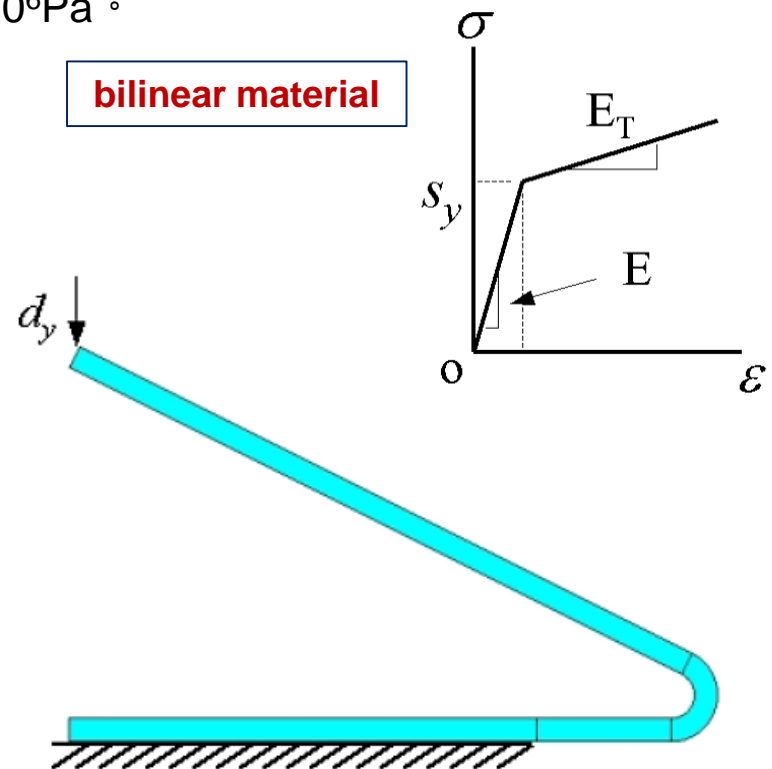
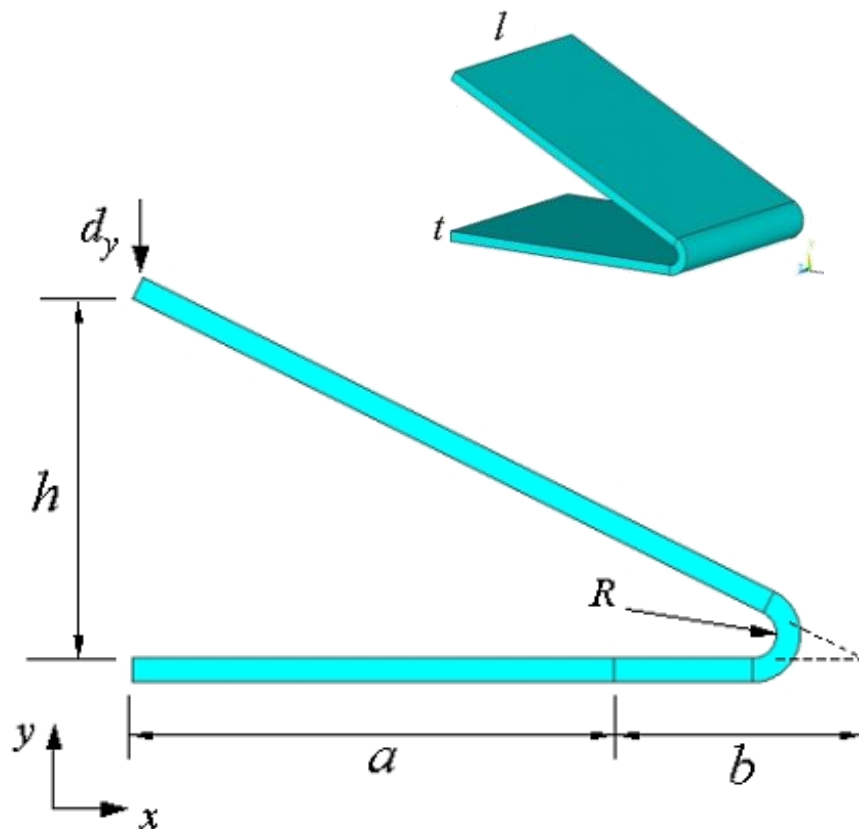


Nonlinear – Ex.12-1

殘留應力分析

如圖所示類似彈簧片的結構，其尺寸為 $l=0.02\text{m}$ ， $h=0.015\text{m}$ ， $a=0.02\text{m}$ ， $b=0.01\text{m}$ ，圓角 $R=0.001\text{m}$ ，厚度 $t=0.001\text{m}$ 。邊界條件如圖，長度 a 之底面部分全部拘束固定，當給定之 y 方向位移 $d_y=-0.002\text{m}$ 時，該結構若有塑性變形，求出移除負荷後的殘留變形。

(1) 材料為 **bilinear material**，楊氏模數 $E=210000 \times 10^6 \text{Pa}$ ，其真應力應變曲線如圖之 BISO 曲線， $E_T=30000 \times 10^6 \text{Pa}$ ，普松比 $\nu=0.3$ ，降伏強度 $S_y=200 \times 10^6 \text{Pa}$ 。



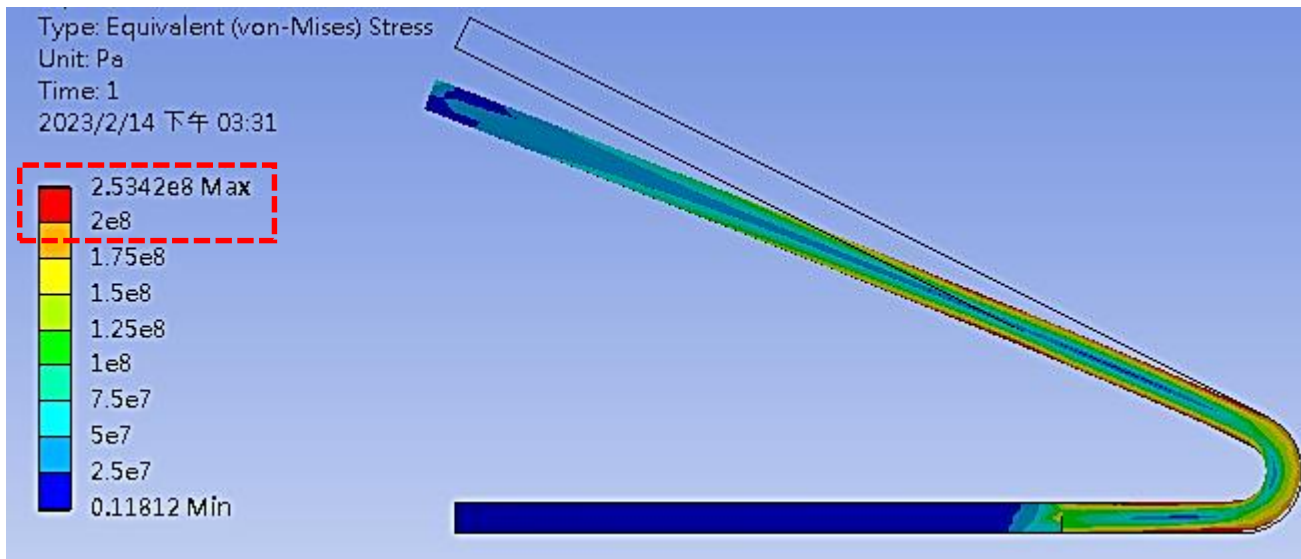
Nonlinear – Ex.12-1

學習目標

- 材料性質設定
- Form new part
- Mesh-Sweep
- 大變形

Step. 1

bilinear material



最大應力超過降伏
→發生塑性變形

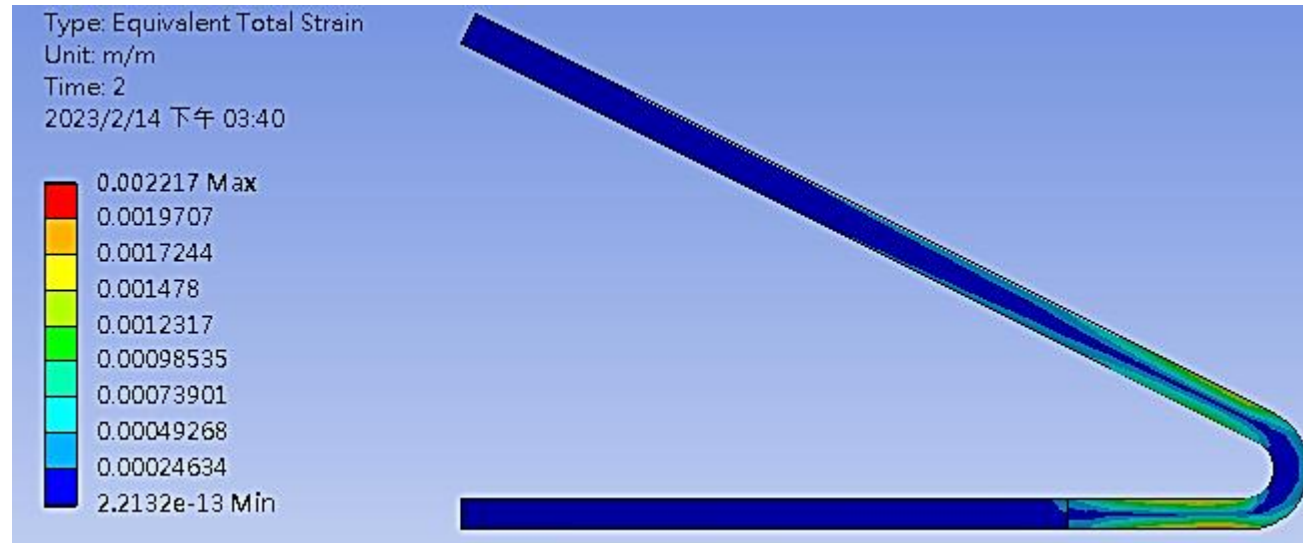
等效應力
Equivalent Stress

Nonlinear – Ex.12-1

學習目標

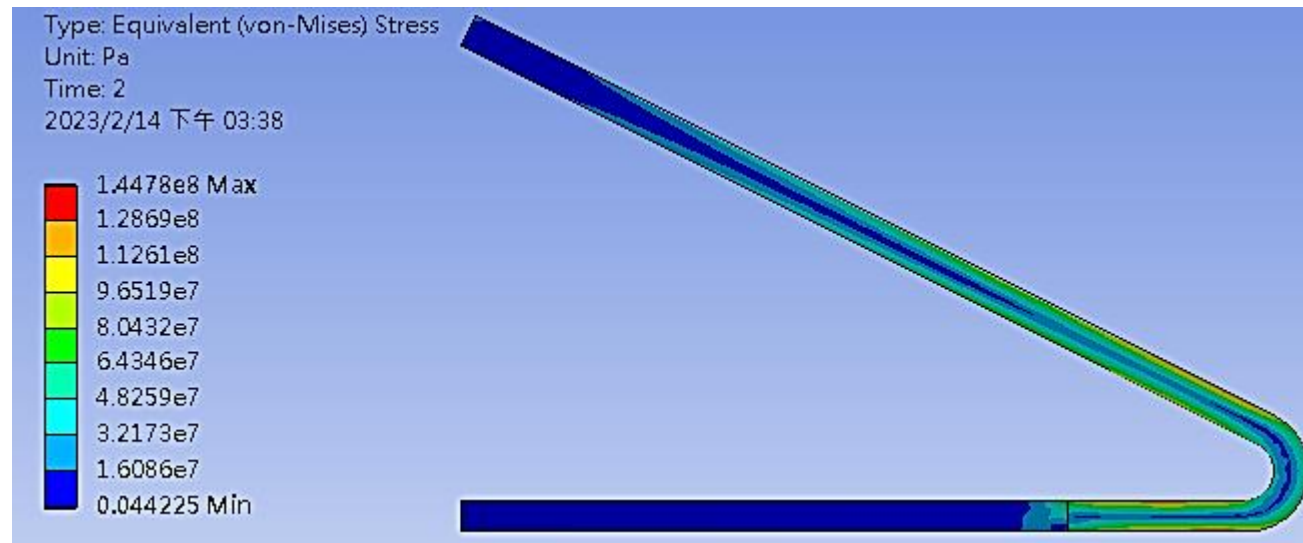
- 材料性質設定
- Form new part
- Mesh-Sweep
- 大變形

Step. 2 **bilinear material**



殘留總應變(彈性+塑性)

等效總應變
Equivalent Total Strain



殘留應力

等效應力
Equivalent Stress



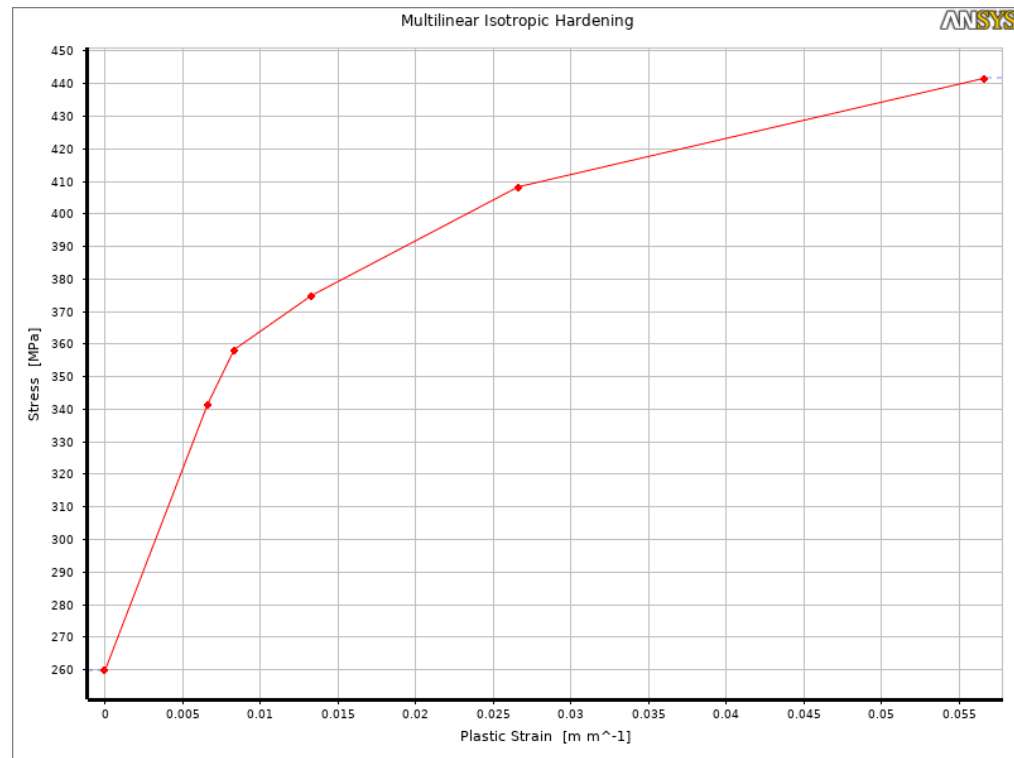
Nonlinear – Ex.12-2

殘留應力分析

如圖所示類似彈簧片的結構，其尺寸為 $l=0.02\text{m}$ ， $h=0.015\text{m}$ ， $a=0.02\text{m}$ ， $b=0.01\text{m}$ ，圓角 $R=0.001\text{m}$ ，厚度 $t=0.001\text{m}$ 。邊界條件如圖，長度 a 之底面部分全部拘束固定，當給定之 y 方向位移 $d_y=-0.004\text{m}$ 時，該結構若有塑性變形，求出移除負荷後的殘留變形。

(2) 材料為 **multilinear material**，數據採用自文獻，楊氏模數 $E=71200\text{MPa}$ ，普松比 $\nu=0.31$ ，降伏強度 $S_y=260\text{MPa}$ ，真應力應變曲線原為一實際曲線，經 MISO 之多直線段簡化且輸入 ANSYS 後如圖，各點座標如下所示。

multilinear material



- 1 (0, 260)
- 2 (0.0066, 341.68)
- 3 (0.0083, 358.34)
- 4 (0.0133, 375.01)
- 5 (0.0266, 408.34)
- 6 (0.0566, 441.68)

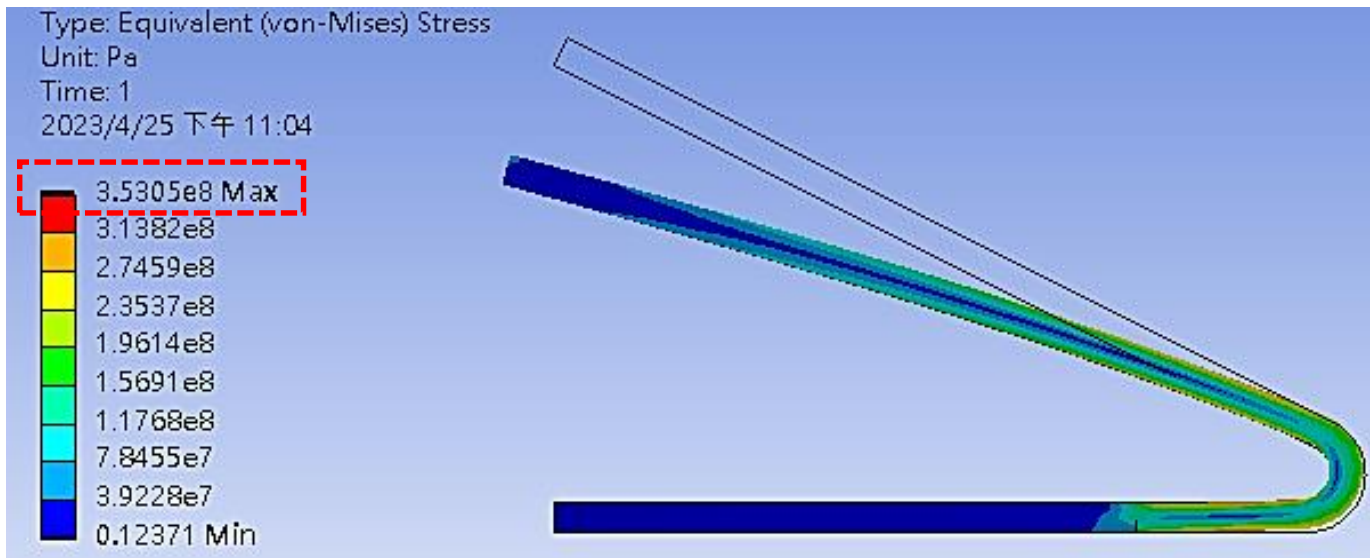
Nonlinear – Ex.12-2

學習目標

- 材料性質設定
- Form new part
- Mesh-Sweep
- 大變形

Step. 1

multilinear material



最大應力超過降伏
→ 發生塑性變形

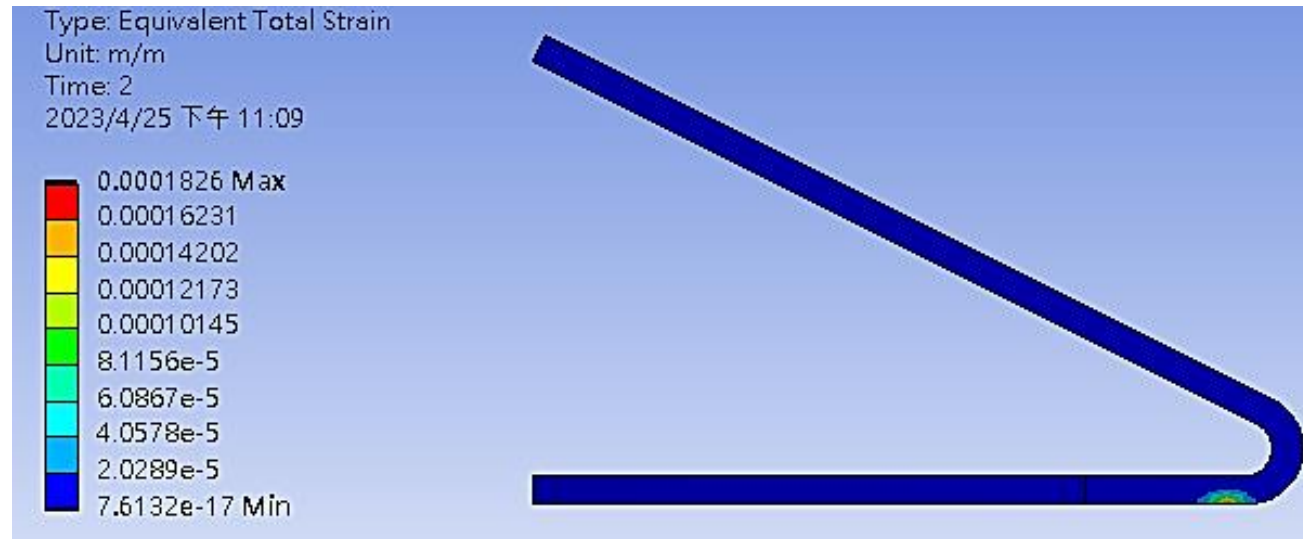
等效應力
Equivalent Stress

Nonlinear – Ex.12-2

學習目標

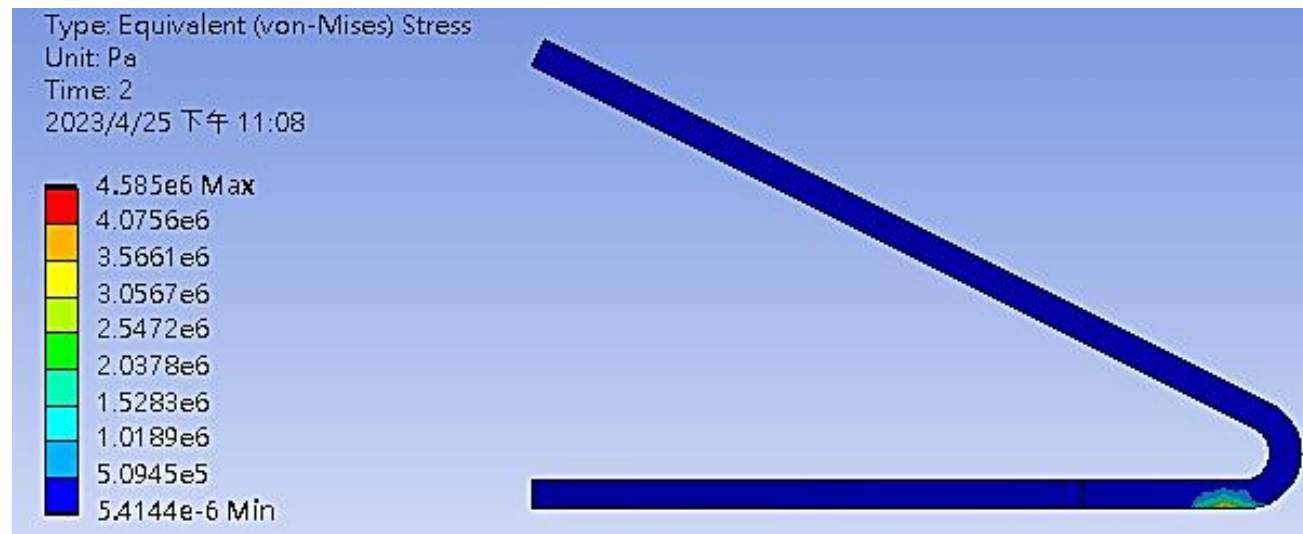
- 材料性質設定
- Form new part
- Mesh-Sweep
- 大變形

Step. 2 **multilinear material**



殘留總應變(彈性+塑性)

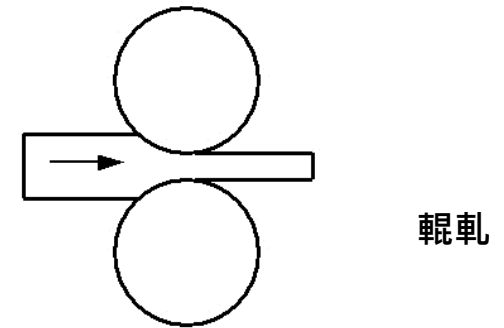
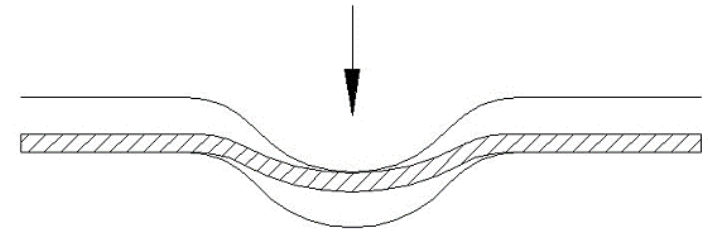
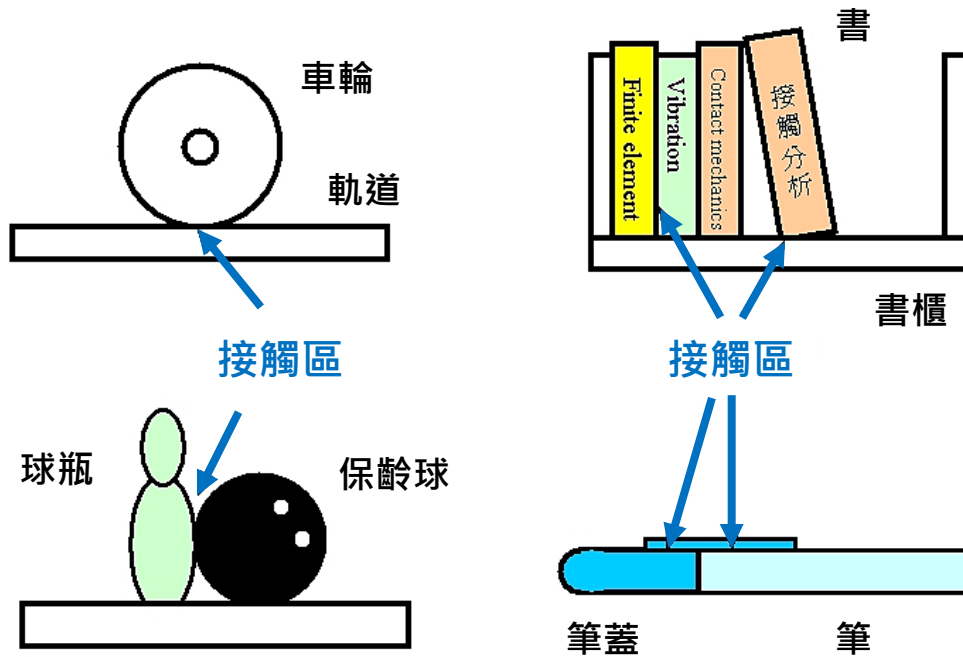
等效總應變
Equivalent Total Strain



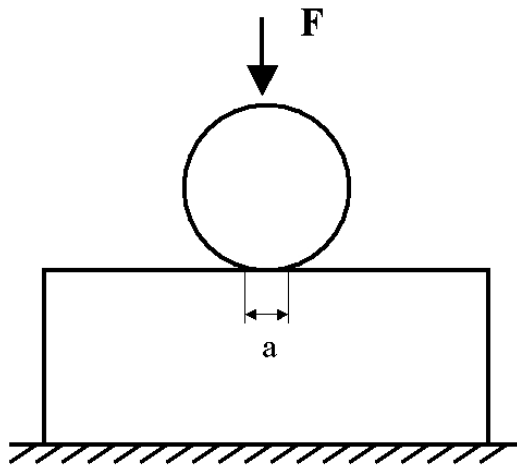
殘留應力

等效應力
Equivalent Stress

Contact Analysis



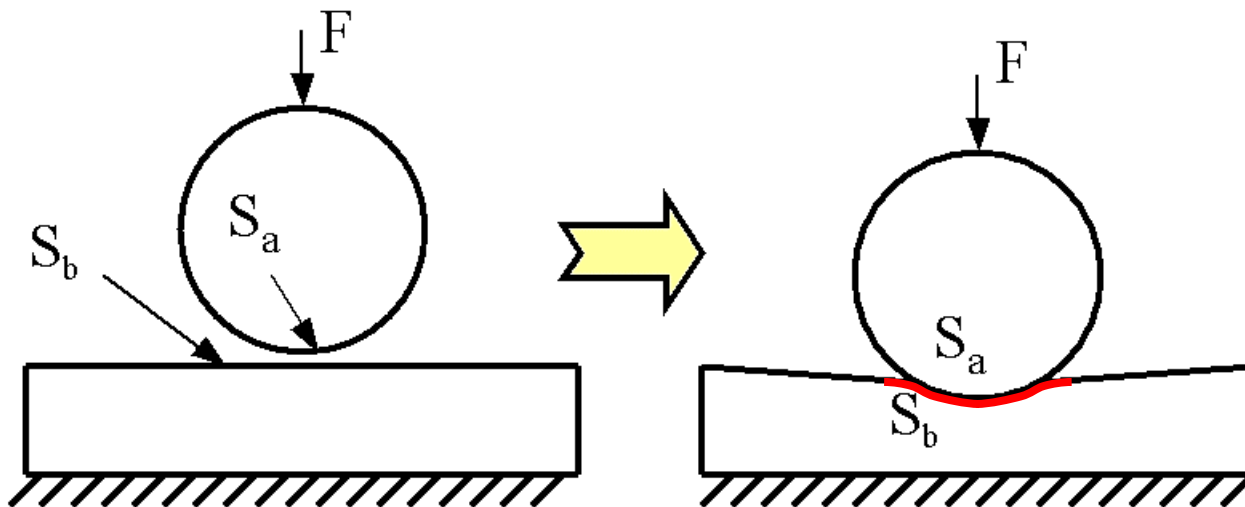
機械加工製程之
接觸問題(塑性變形)



兩物體之
彈性接觸問題

Contact Analysis

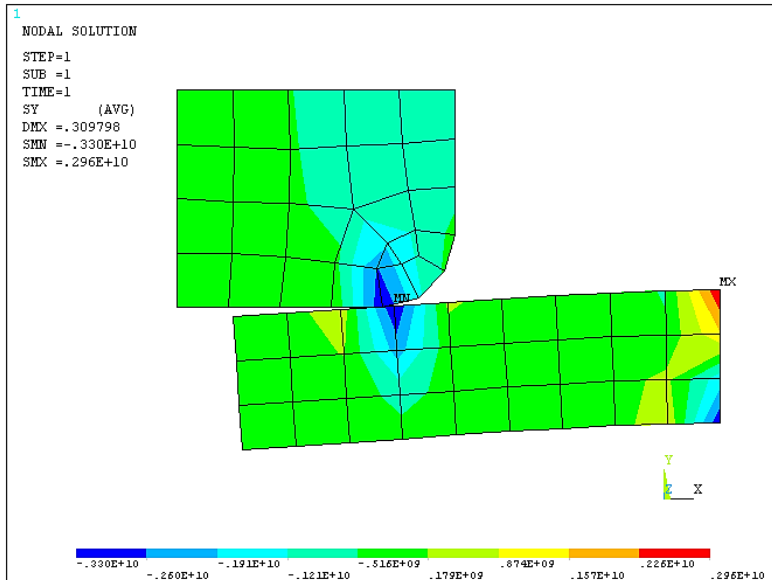
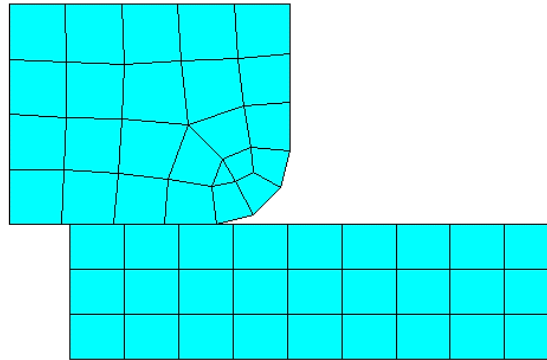
- 有限元素接觸分析是於物體之間的接觸面上加入非貫穿(non-penetration)條件
- 以下圖之兩物體接觸為例，首先須將 S_a 和 S_b 兩個面定義為接觸面，下令兩接觸面不可貫穿，如此一來，只要圓形物體受力變形，便可透過兩接觸面 S_a 和 S_b 將力量傳至矩形物體，使得矩形物體也跟著變形，即完成了接觸分析
- ANSYS是利用接觸元素(contact elements)來模擬接觸面，只要接觸區域的接觸元素一被建立，計算時就會考慮到接觸條件



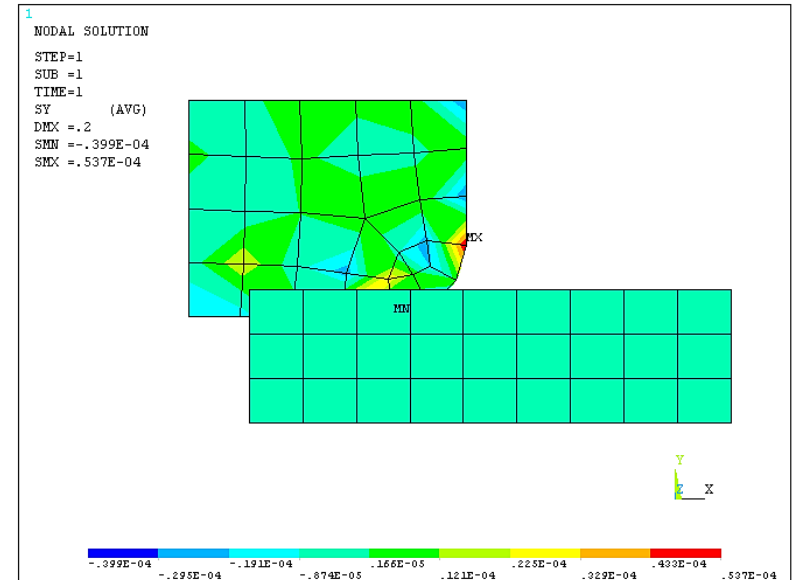
Contact Analysis



ELEMENTS



合理之接觸分析結果



不合理之接觸分析結果
(未建立接觸元素)

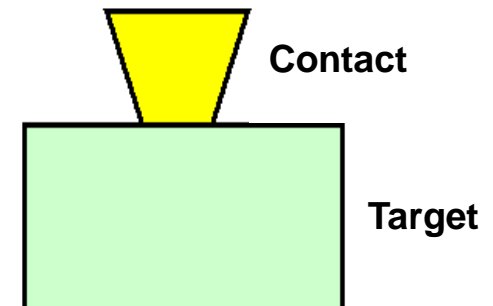
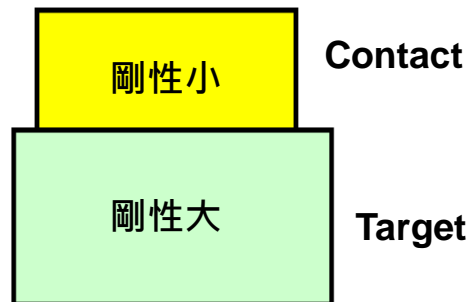
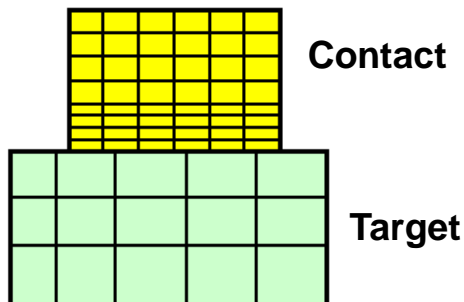
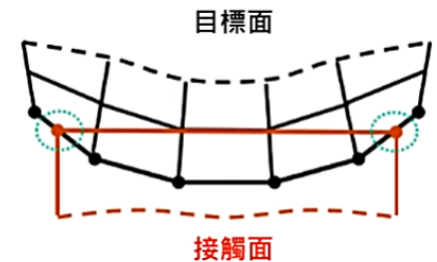
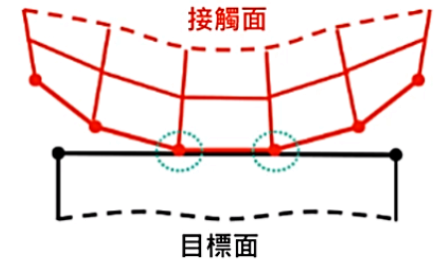


Contact Analysis

- 在ANSYS定義中，目標面(Target surface)的節點可以穿透接觸面(Contact surface)，接觸面的節點則不可穿透目標面

- 接觸對之接觸元素和目標元素建立原則

| 目標面(Target surface) | 接觸面(Contact surface) |
|---------------------|----------------------|
| 網格較粗 | 網格較細 |
| 剛性較大(硬) | 剛性較小(軟) |
| 面積顯著較大(平面、凹面) | 面積顯著較小(尖、凸面) |

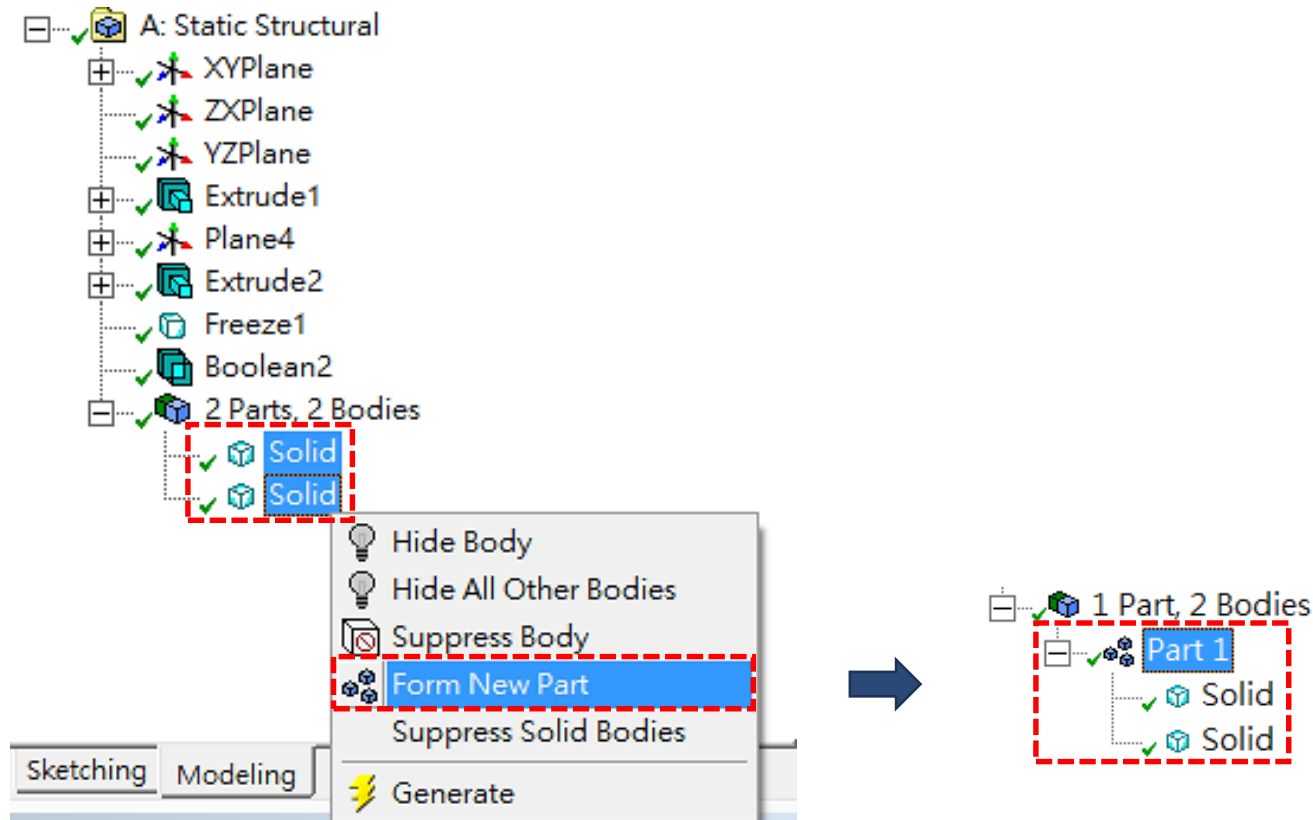


Introduction of ANSYS Workbench

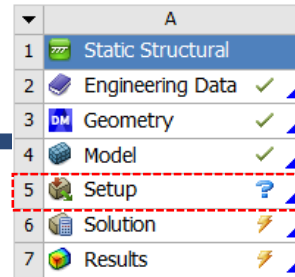
| A | |
|---|-------------------|
| 1 | Static Structural |
| 2 | Engineering Data |
| 3 | DM Geometry |
| 4 | Model |
| 5 | Setup |
| 6 | Solution |
| 7 | Results |

■ 介面條件設定

- 模型為組合件時，若要組合件間能共用面，達到力量直接傳遞時，必須將此部份組件形成一個群組>**From New part**
- 若要組合件間能有各自的面，達到**contact**效果時，則不須進行此動作，模型匯入後軟體會自動判斷出非連續面之部份



Introduction of ANSYS Workbench



■ 接觸(Contact)設定

➤ 軟體會自動偵測到不同part之界面，並於**Connection**中顯示所有之**contact**區域

➤ 接觸行為設定

✓ Bonded

- 預設項目，沒有相對滑動和分離，會忽略初始穿刺(**penetration**)，模擬為相互連接

✓ No Separation

- 類似Bonded，僅適用於面(3D)或邊(2D)之接觸，沒有相對分離，僅可延接觸面有些微無摩擦滑動

✓ Frictionless

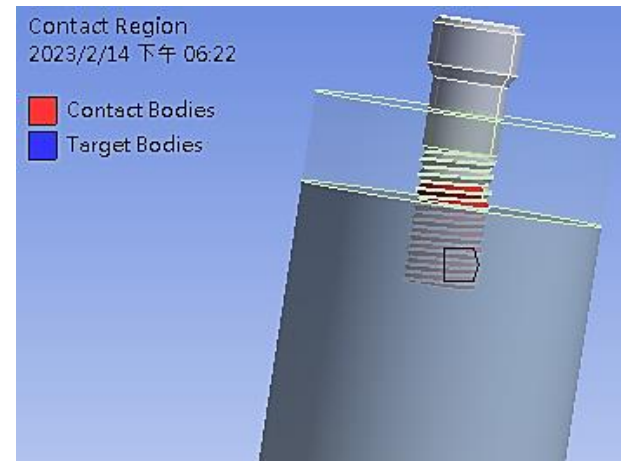
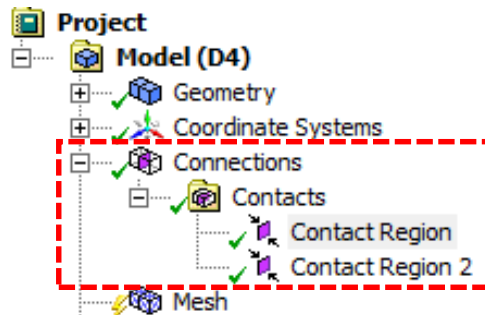
- 此為單邊接觸，假設摩擦係數為0，允許相對滑動，出現分離時法向量壓力為0，法向會分離

✓ Rough

- 類似Frictionless，有摩擦係數，無相對滑動，法向會分離

✓ Frictional

- 有摩擦係數，有相對滑動，法向會分離



Contact – Ex.13

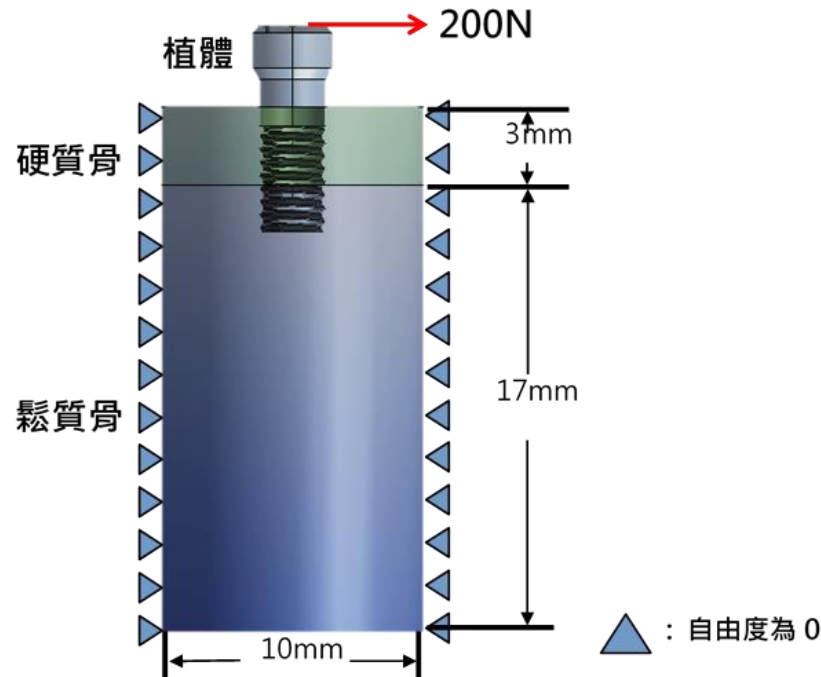


人工牙根分析

請構出硬質骨與鬆質骨圓柱模型，尺寸如圖所示，並將外部CAD軟體建構出之植體檔(screw.igs)匯入，施加側向力200N負載於植體頂部(已於植體頂部建構一凹點特徵)上，並設定硬質骨/鬆質骨外側自由度為0(如下圖)。各材料特性：硬質骨(楊氏係數17000MPa；蒲松比0.3)、鬆質骨(楊氏係數200MPa；蒲松比0.2)及植體(鈦合金楊氏係數110000MPa；蒲松比0.33)，採用四面體網格，網格尺寸：植體0.5mm、硬質骨0.8mm、鬆質骨1.0mm、硬質骨內側螺紋面0.5mm。觀察硬質骨最大主應變(Maximum Principal strain)及植體最大等效應力(von-Mises stress)情形。

(1)植體與硬質骨/鬆質骨界面未結合(unbonded)狀態之設定(模擬植體剛植入骨頭)

(2)植體與硬質骨/鬆質骨界面結合(bonded)狀態之設定(模擬植體與骨頭已骨整合)



Contact – Ex.13

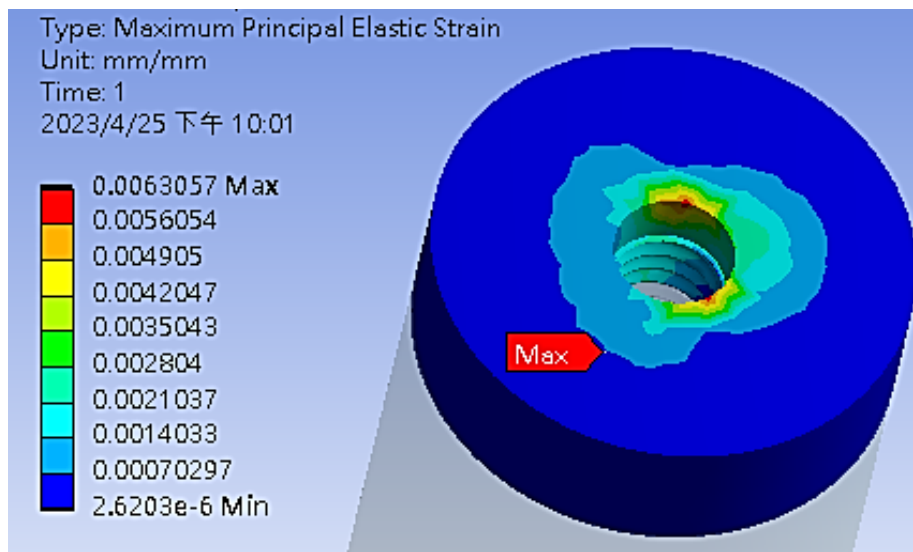
- 學習目標
- 外部模型導入
 - Offset plane
 - Move
 - Contact設定

(1) Unbonded



Screw

等效應力
Equivalent Stress



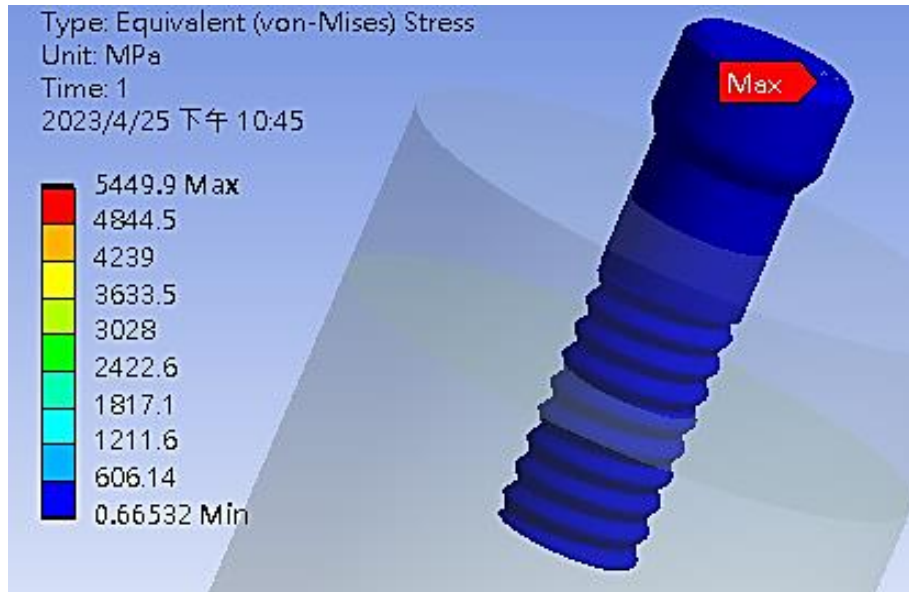
Cortical Bone

最大主應變
Maximum Principal Strain

Contact – Ex.13

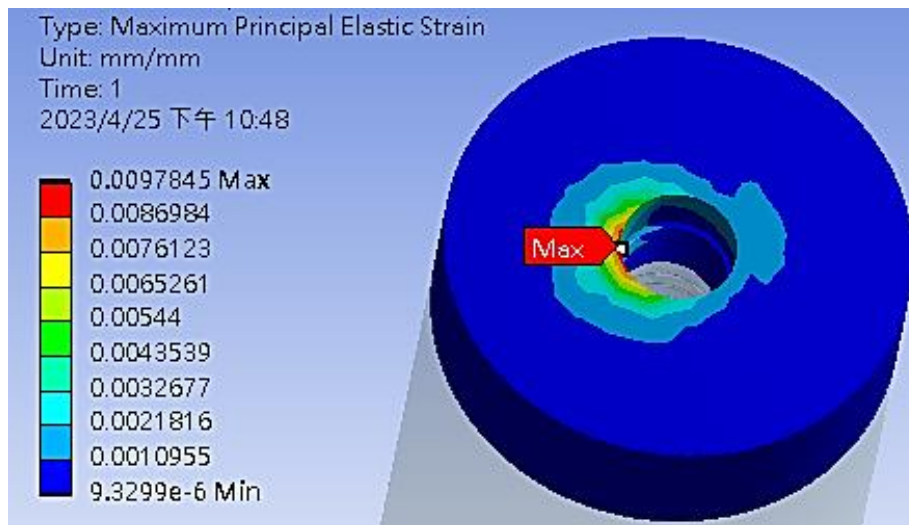
- 學習目標
- 外部模型導入
 - Offset plane
 - Move
 - Contact設定

(2) Bonded



Screw

等效應力
Equivalent Stress



Cortical Bone

最大主應變
Maximum Principal Strain

Nonlinear & Contact – Ex.14 (來源：成功大學李輝煌教授)

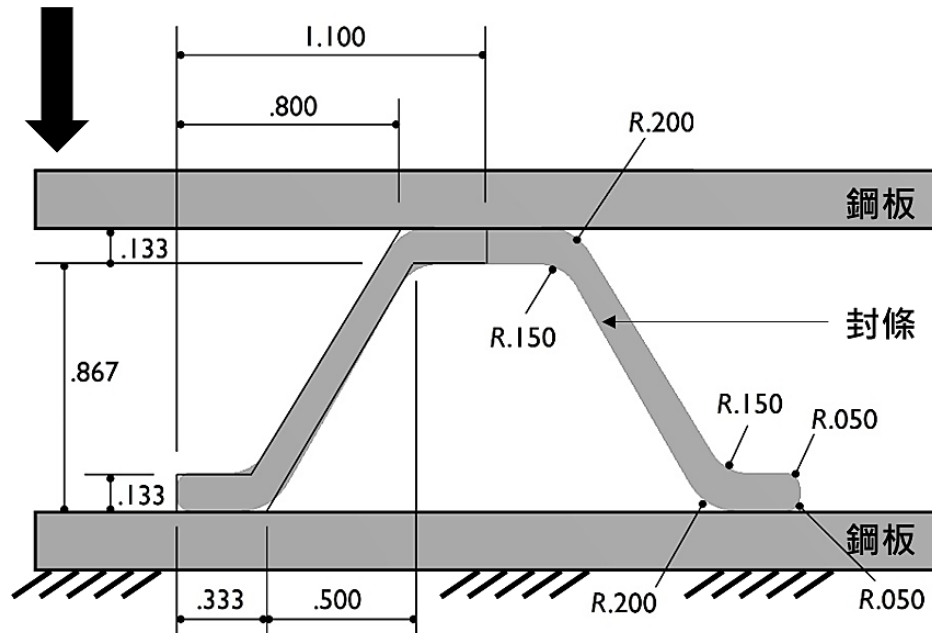


非線性材料

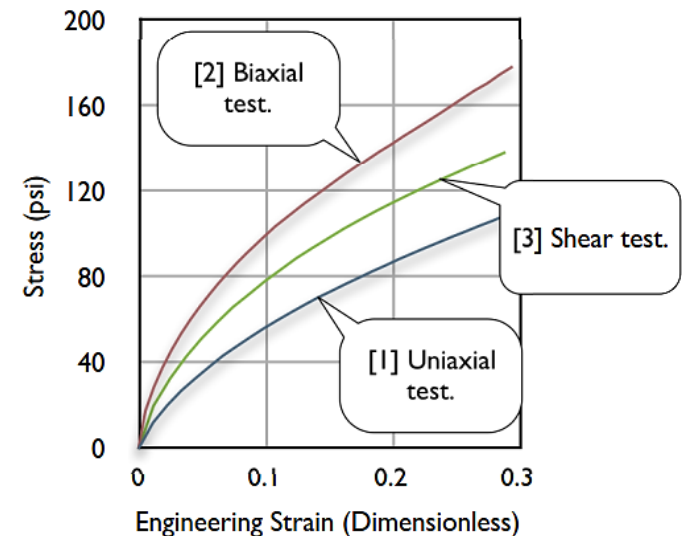
如圖為一冰箱門封元件，由兩鋼板及一長條形封條組成。封條為超彈性材料，其材料特性由實驗量測得到(TESTDATA)，包含單軸/雙軸拉伸測試及剪力測試。

本習題將學習如何藉由實驗數據輸入得到超彈性材料特性，並模擬封條受兩鋼板擠夾之力學行為。此次將以2D進行模型建構，並以PLANE STRAIN進行模擬後觀察其最大主應力(變)/最小主應力(變)/剪應力(變)。

位移0.85"



單位：inch



Nonlinear & Contact – Ex.14

學習目標

- 材料data匯入
- Hyperelastic

Type: Maximum Principal Stress

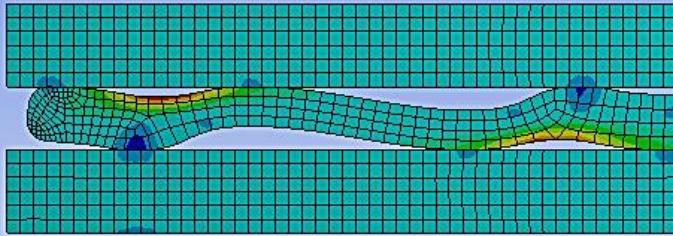
Unit: psi

Time: 1

2023/2/18 上午 05:12

最大主應力

135.59 Max
115.78
95.967
76.155
56.344
36.533
16.721
-3.09
-22.901
-42.713 Min



Type: Maximum Principal Elastic Strain

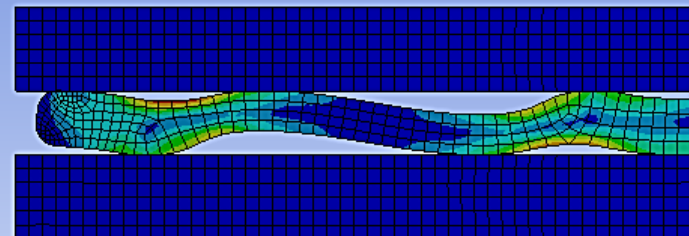
Unit: in/in

Time: 1

2023/2/18 上午 05:18

最大主應變

0.16757 Max
0.14895
0.13033
0.11171
0.093095
0.074476
0.055857
0.037238
0.018619
0 Min



Type: Minimum Principal Stress

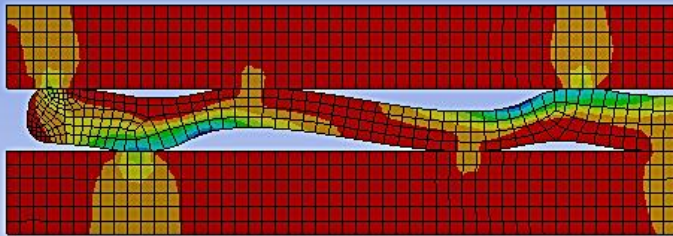
Unit: psi

Time: 1

2023/2/18 上午 05:15

最小主應力

6.2675 Max
-6.8068
-19.881
-32.956
-46.03
-59.104
-72.179
-85.253
-98.327
-111.4 Min



Type: Minimum Principal Elastic Strain

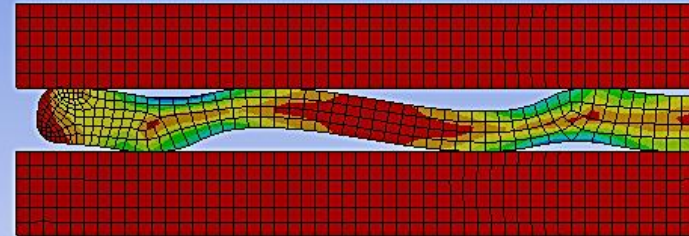
Unit: in/in

Time: 1

2023/2/18 上午 05:19

最小主應變

0 Max
-0.01865
-0.0373
-0.05595
-0.0746
-0.09325
-0.1119
-0.13055
-0.1492
-0.16785 Min



Type: Shear Stress(XY Plane)

Unit: psi

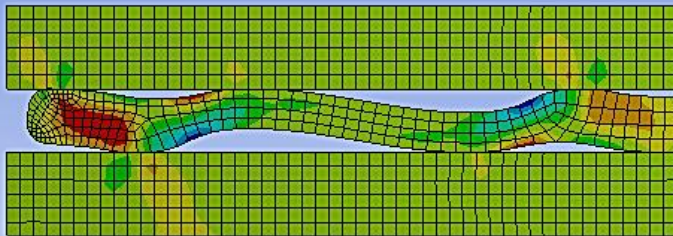
Global Coordinate System

Time: 1

2023/2/18 上午 05:15

剪應力

21 Max
14.577
8.1539
1.7309
-4.6922
-11.115
-17.538
-23.961
-30.384



Type: Shear Elastic Strain(XY Plane)

Unit: in/in

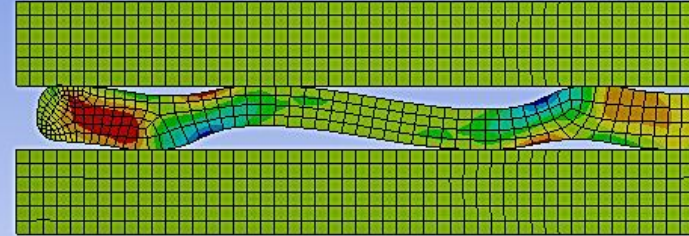
Global Coordinate System

Time: 1

2023/2/18 上午 05:20

剪應變

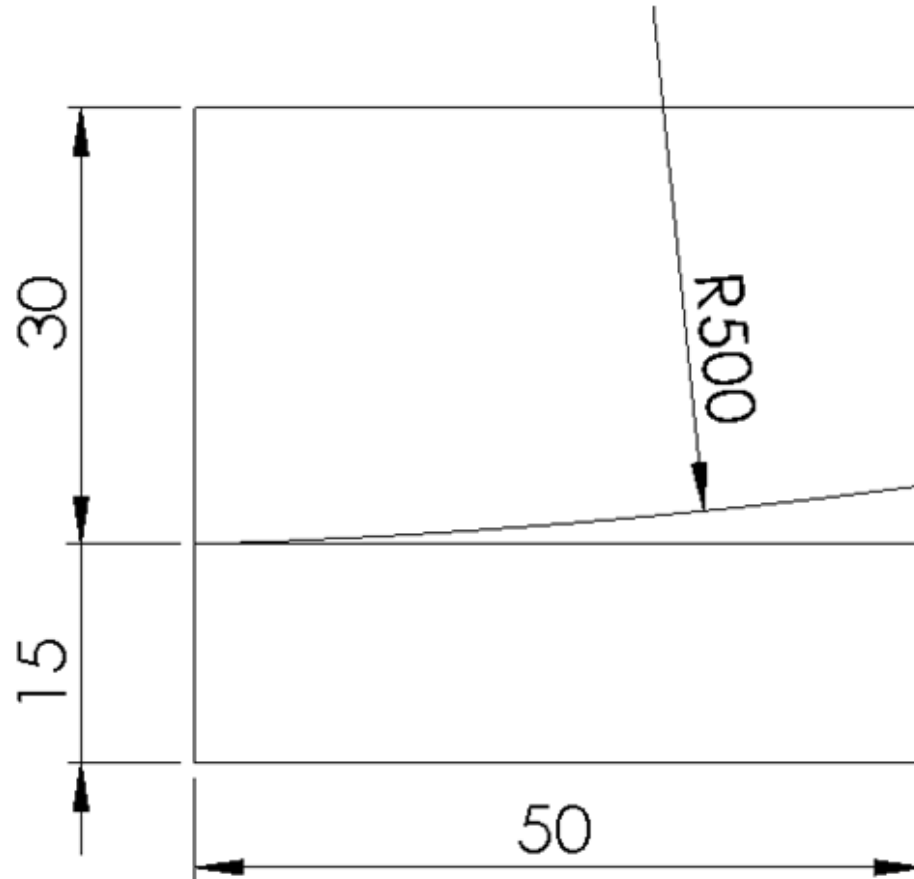
0.10479 Max
0.072577
0.040369
0.0081613
-0.024047
-0.056255
-0.088463
-0.12067
-0.15288



Nonlinear & Contact – Ex.15

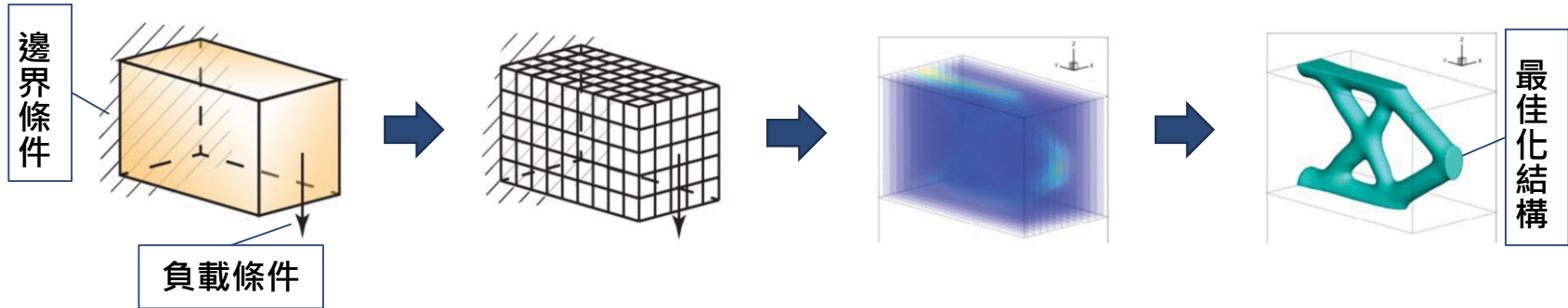


2D模型如圖所示，其為剛性接觸的兩物體且下端整面為固定並於上端邊線受一5MPa之壓力，請針對該模型進行接觸剛性分析。

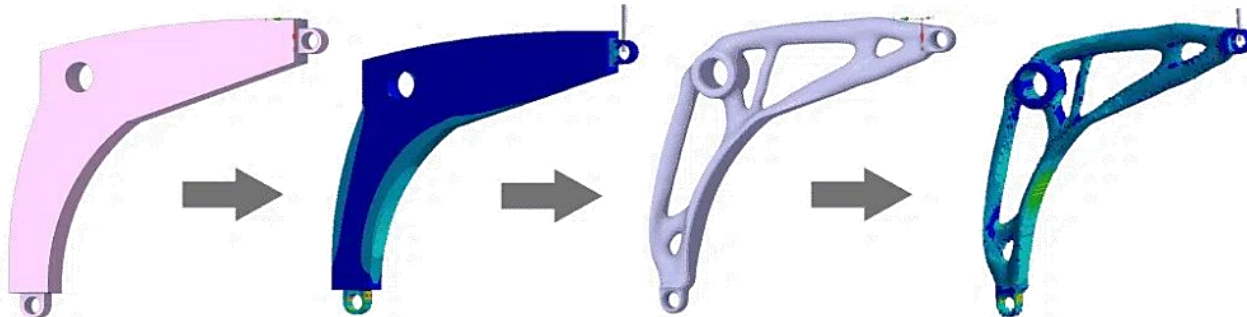


結構最佳化

- **拓樸最佳化(Topology Optimization)**是一種結構優化技術，可**自行定義設計範圍(Design Domain)**，根據給定的**限制條件**與**目標函數**，解出符合給定條件之最佳結構



- 拓樸最佳化結合**有限元素法**及**最佳化演算法**，將**最佳密度值**分配給定義域中的每個元素，求得該結構之最佳材料分布情形
- 可實現在一定的結構強度要求下，將材料做出最有效之配置，以節省不必要的材料達到**輕量化**之目標

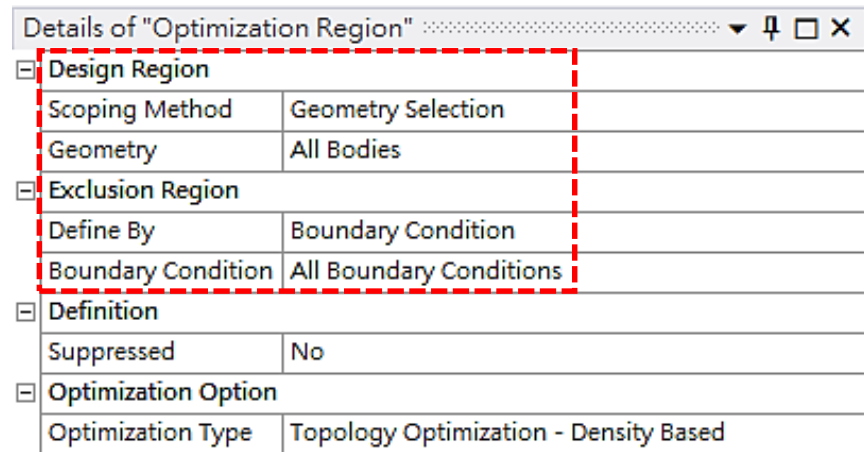
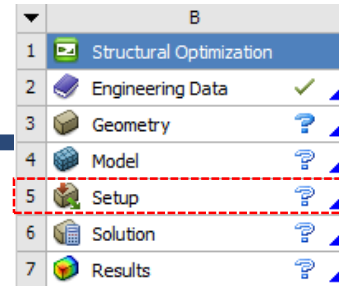
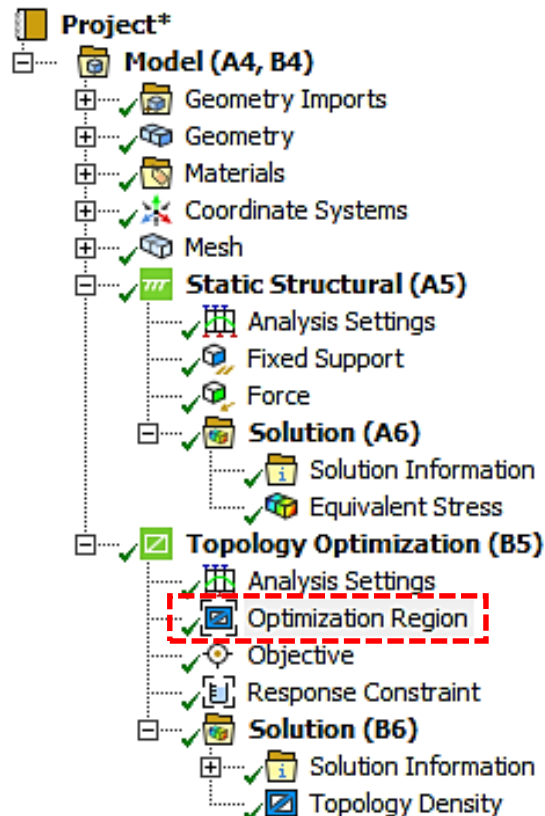


Introduction of ANSYS Workbench

■ Topology Optimization (Structural Optimization)

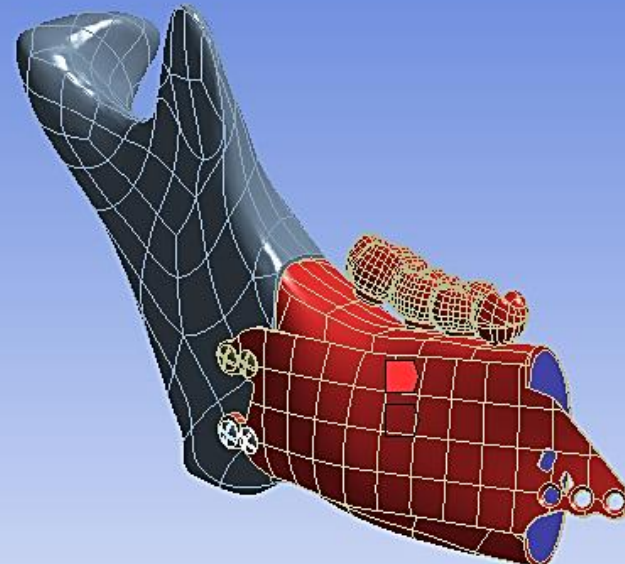
➤ 設計範圍 - Optimization Region

- ✓ Design Region
- ✓ Exclusive Region



B: Topology Optimization
Optimization Region
Iteration Number: N/A
2023/2/25 上午 07:45

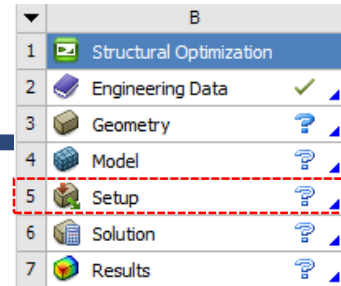
■ Design Region: Topology
■ Exclusion Region



Introduction of ANSYS Workbench

■ Topology Optimization (Structural Optimization)

- 目標函數 - Objective
- 限制條件 - Response Constraint



Objective

Right click on the grid to add, modify and delete a row.

| Enabled | Response Type | Goal | Criterion | Formulation | Environment Name | Weight | Multiple Sets | Start Step | End Step |
|-------------------------------------|---------------|----------|-----------|--------------------|-------------------|--------|---------------|------------|----------|
| <input checked="" type="checkbox"/> | Compliance | Minimize | N/A | Program Controlled | Static Structural | N/A | Enabled | 1 | 1 |

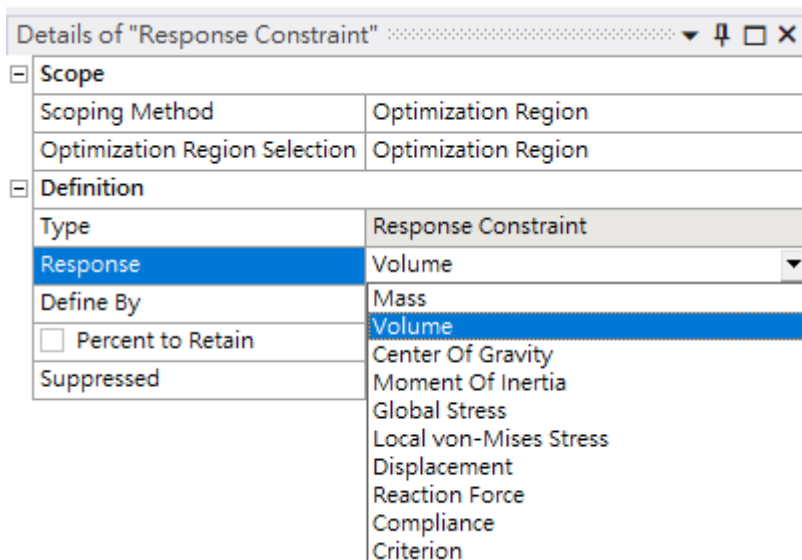
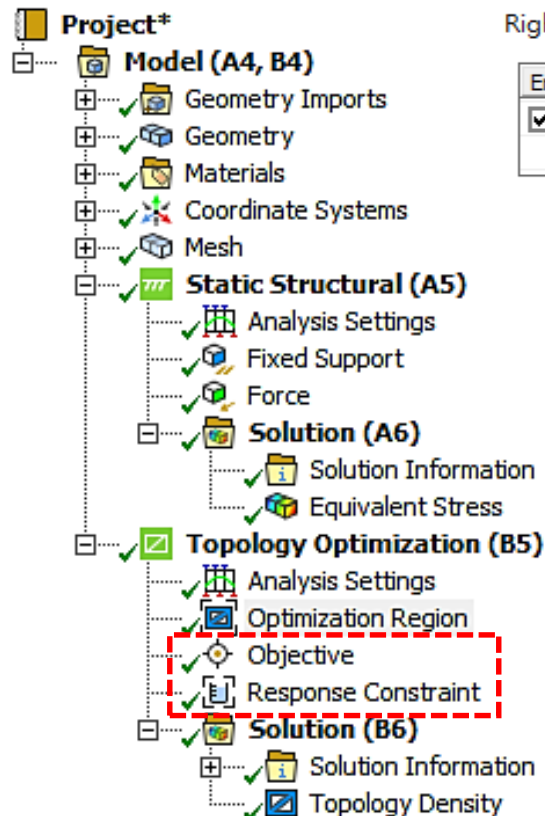
Mass

Volume

Compliance

Stress

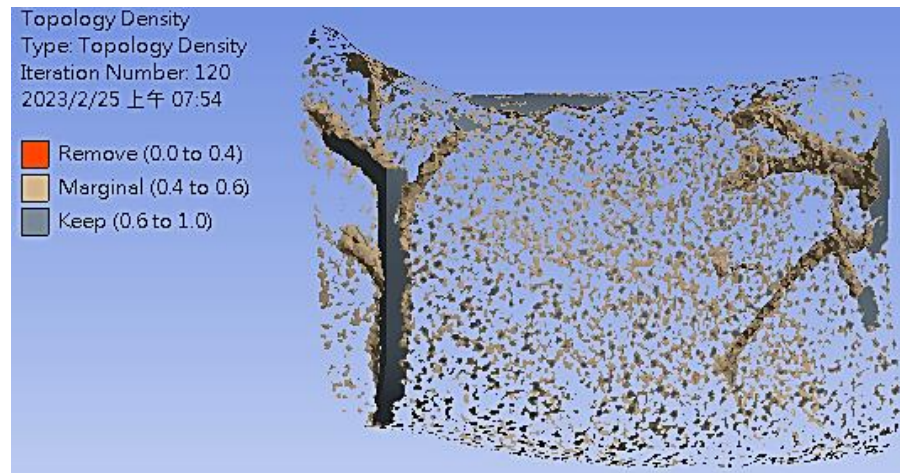
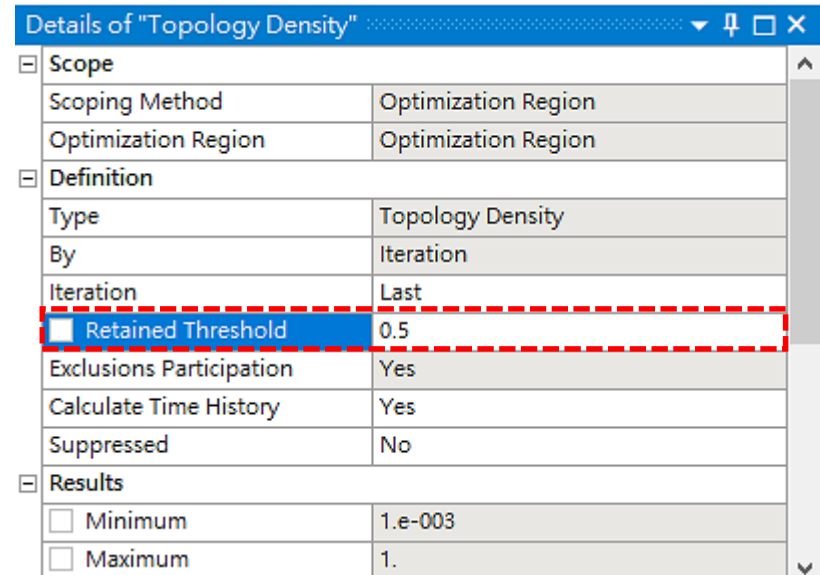
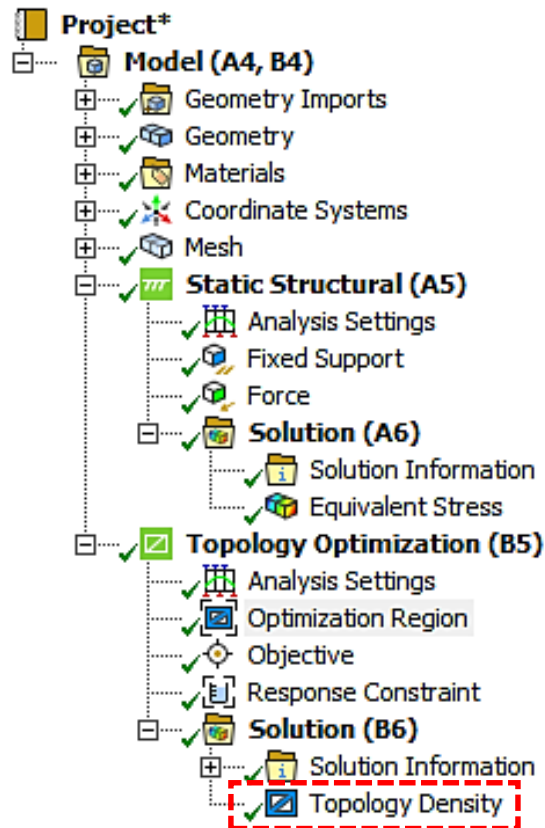
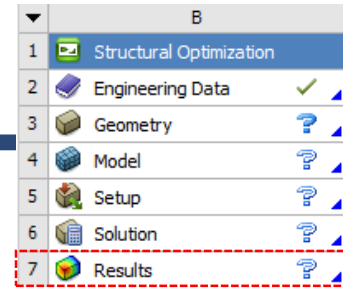
Criterion



Introduction of ANSYS Workbench

■ Structural Optimization (Topology Optimization)

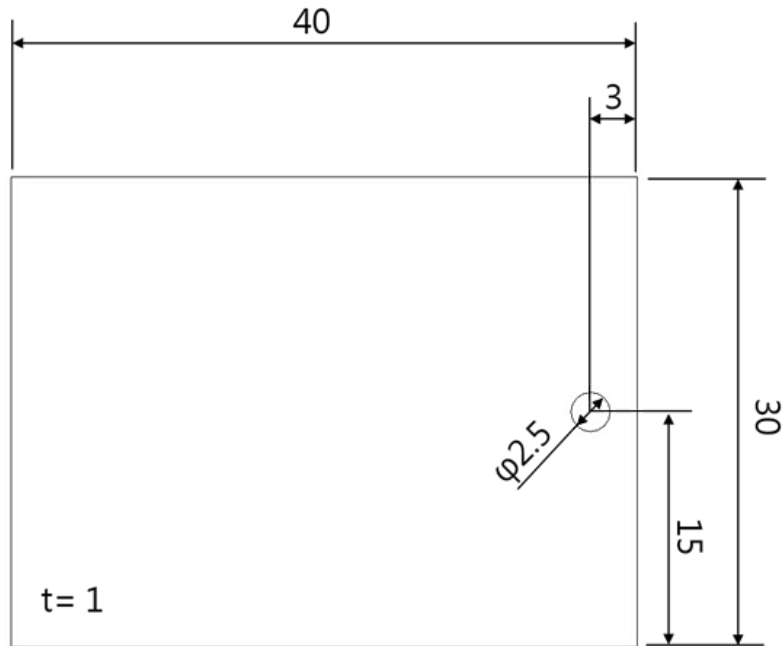
➤ 最佳結構 - Topology Density(拓樸密度)



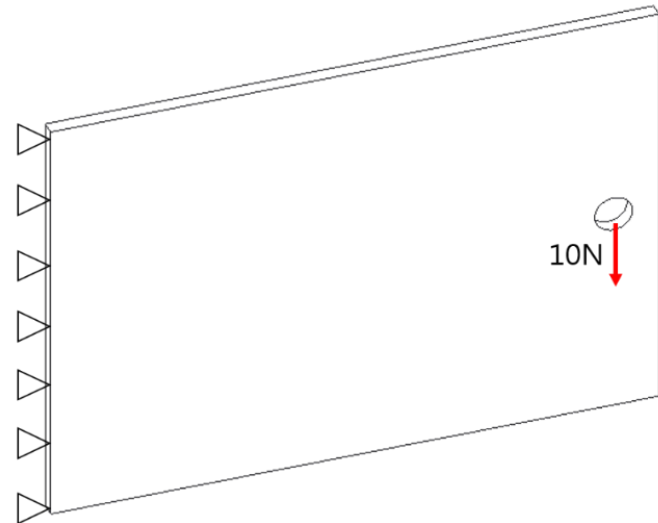
Structural Optimization – Ex.16



平板模型如圖所示，請針對該模型進行拓撲最佳化(Topology Optimization)，最佳化目標為剛度最大情形下，減少40%體積。材料使用Structural steel，網格形式採用四面體(Tetrahedrons)，網格尺寸為1mm，平板左側固定並於圓孔曲面上施以力量(Y方向，向下10N)。



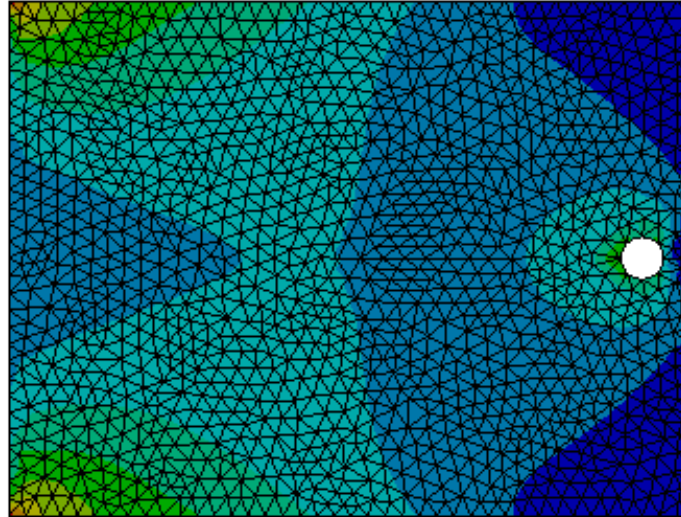
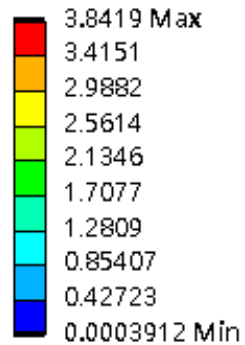
Unit : mm



Structural Optimization – Ex.16

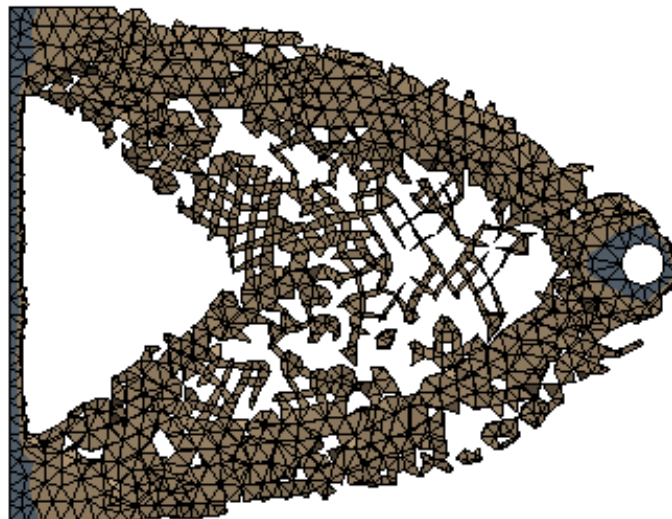
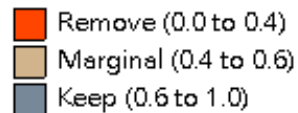
學習目標
• 拓樸最佳化設定

Equivalent Stress
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1 s
2023/2/25 上午 07:02



等效應力
Equivalent Stress

Topology Density
Type: Topology Density
Iteration Number: 20
2023/2/25 上午 07:05



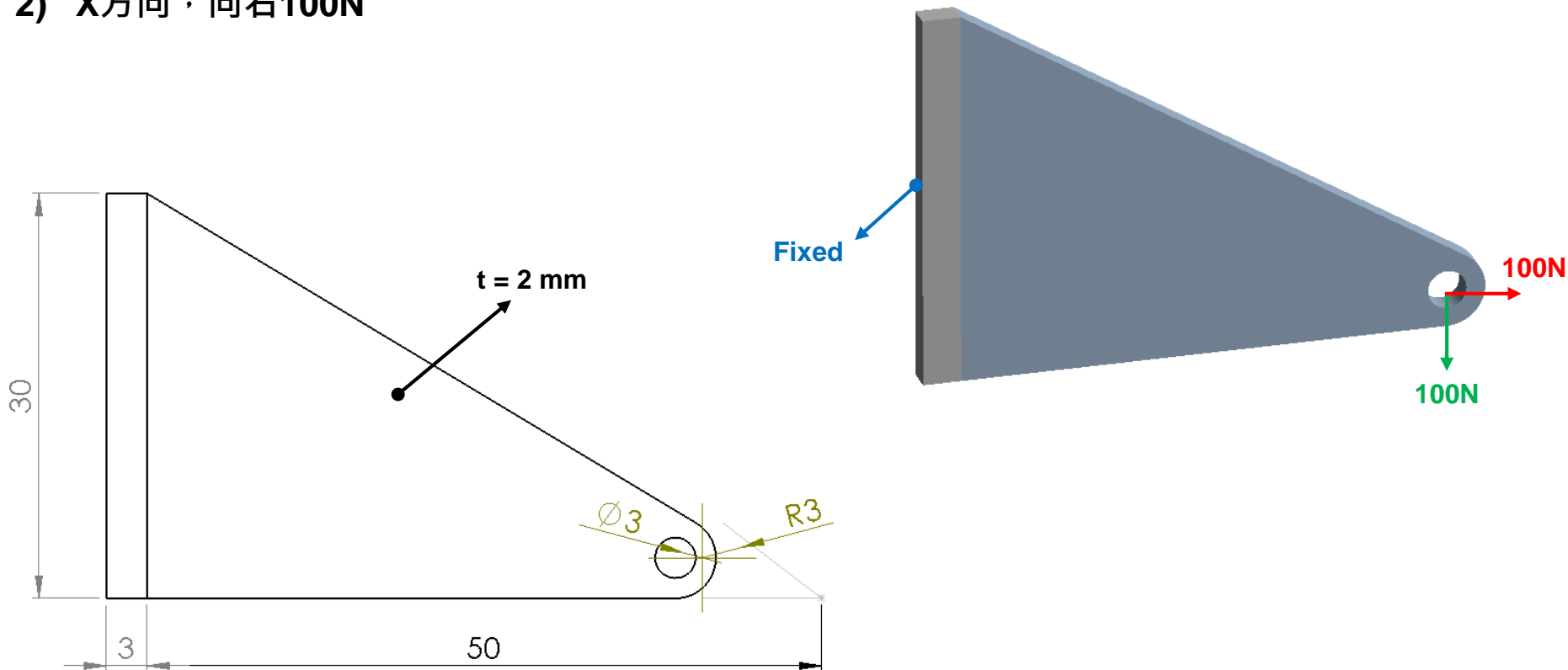
拓樸密度結構
Topology Density



Design Validation – Ex.17

三角bracket模型如圖所示，請針對該模型右側區塊進行拓撲最佳化(Topology Optimization)，最佳化目標為剛度最大情形下，減少50%體積。材料使用Structural steel，網格尺寸為1mm，左側固定，右側圓孔曲面上施以力量，並利用Design Validation將最佳化結構再次進行力學分析。試比較不同力量下，最佳化結果與結構應力分析結果差異。

- 1) Y方向，向下100N
- 2) X方向，向右100N



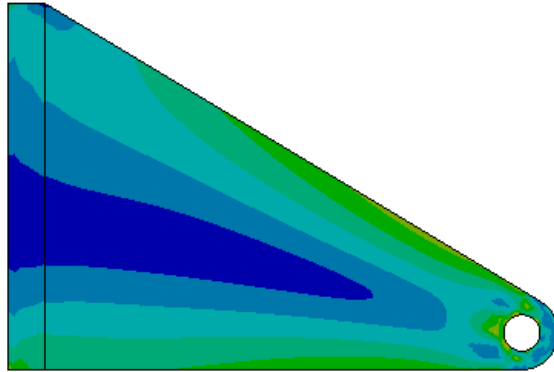
Design Validation – Ex.17

學習目標

- Design Validation
- SpaceClaim基礎修模

Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1 s
2023/3/23 上午 07:49

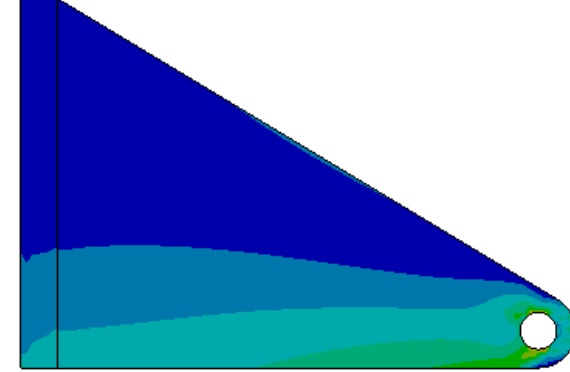
39.22 Max
34.893
30.565
26.238
21.911
17.583
13.256
8.9285
4.6011
0.27373 Min



原始模型等效應力(向下)
Equivalent Stress

Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1 s
2023/3/23 上午 07:59

24.012 Max
21.349
18.686
16.024
13.361
10.698
8.0355
5.3728
2.7101
0.047378 Min



原始模型等效應力(向右)
Equivalent Stress

Type: Topology Density
Iteration Number: 23
2023/3/23 上午 07:50

Remove (0.0 to 0.4)
Marginal (0.4 to 0.6)
Keep (0.6 to 1.0)



拓樸密度結構(向下)
Topology Density

Type: Topology Density
Iteration Number: 10
2023/3/23 上午 07:59

Remove (0.0 to 0.4)
Marginal (0.4 to 0.6)
Keep (0.6 to 1.0)



拓樸密度結構(向右)
Topology Density

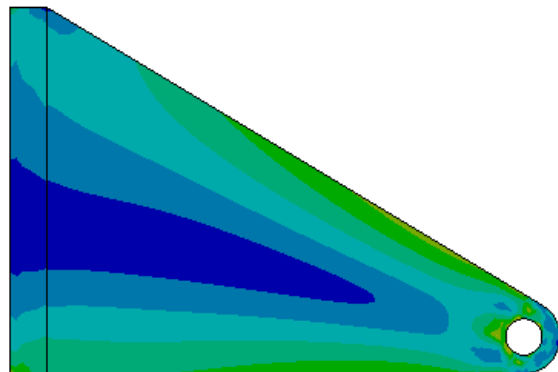
Design Validation – Ex.17

學習目標

- Design Validation
- SpaceClaim基礎修模

Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1 s
2023/3/23 上午 07:49

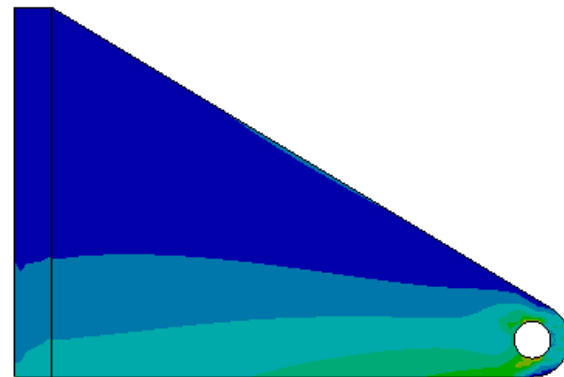
39.22 Max
34.893
30.565
26.238
21.911
17.583
13.256
8.9285
4.6011
0.27373 Min



原始模型等效應力(向下)
Equivalent Stress

Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1 s
2023/3/23 上午 07:59

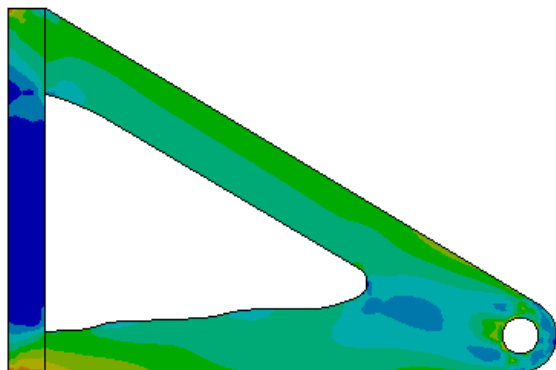
24.012 Max
21.349
18.686
16.024
13.361
10.698
8.0355
5.3728
2.7101
0.047378 Min



原始模型等效應力(向右)
Equivalent Stress

Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1 s
2023/3/23 上午 07:55

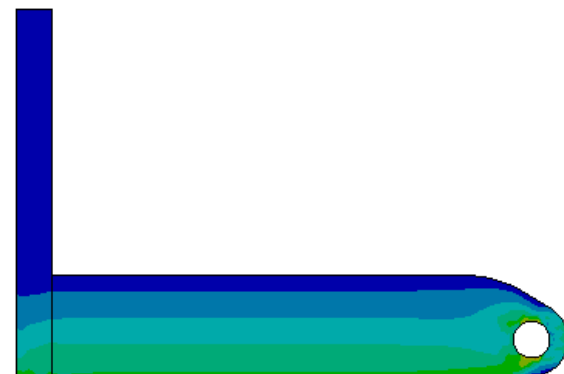
39.616 Max
35.214
30.813
26.411
22.009
17.608
13.206
8.8046
4.403
0.0014006 Min



拓樸結構(向下)等效應力
Equivalent Stress

Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1 s
2023/3/23 上午 07:56

23.762 Max
21.122
18.482
15.842
13.201
10.561
7.9208
5.2805
2.6403
1.9065e-6 Min



拓樸結構(向右)等效應力
Equivalent Stress