## CHAPTER

MECHANICS OF MATERIALS

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Transformations of Stress and Strain

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## MECHANICS OF MATERIALS

## Introduction




- The most general state of stress at a point may be represented by 6 components,

$$
\begin{array}{ll}
\sigma_{x}, \sigma_{y}, \sigma_{z} & \text { normalstresses } \\
\tau_{x y}, \tau_{y z}, \tau_{z x} & \text { shearingstresses } \\
& \left(\text { Note: } \tau_{x y}=\tau_{y x}, \tau_{y z}=\tau_{z y}, \tau_{z x}=\tau_{x z}\right)
\end{array}
$$

- Same state of stress is represented by a different set of components if axes are rotated.
- The first part of the chapter is concerned with how the components of stress are transformed under a rotation of the coordinate axes. The second part of the chapter is devoted to a similar analysis of the transformation of the components of strain.


## MECHANICS OF MATERIALS

## Introduction



- Plane Stress - state of stress in which two faces of the cubic element are free of stress. For the illustrated example, the state of stress is defined by

$$
\sigma_{x}, \sigma_{y}, \tau_{\mathrm{xy}} \text { and } \sigma_{z}=\tau_{z x}=\tau_{z y}=0
$$

- State of plane stress occurs in a thin plate subjected to forces acting in the midplane of the plate.
- State of plane stress also occurs on the free surface of a structural element or machine component, i.e., at any point of the surface not subjected to an external force.



## MECHANICS OF MATERIALS

### 7.1 Transformation of Plane Stress



- Consider the conditions for equilibrium of a prismatic element with faces perpendicular to the $x, y$, and $x$ ' axes.

$$
\begin{aligned}
\Sigma F_{x^{\prime}}=0= & \sigma_{x^{\prime}} \Delta A-\sigma_{x}(\Delta A \cos \theta) \cos \theta-\tau_{x y}(\Delta A \cos \theta) \sin \theta \\
& -\sigma_{y}(\Delta A \sin \theta) \sin \theta-\tau_{x y}(\Delta A \sin \theta) \cos \theta \\
\Sigma F_{y^{\prime}}=0= & \tau_{x^{\prime} y^{\prime}} \Delta A+\sigma_{x}(\Delta A \cos \theta) \sin \theta-\tau_{x y}(\Delta A \cos \theta) \cos \theta \\
& -\sigma_{y}(\Delta A \sin \theta) \cos \theta+\tau_{x y}(\Delta A \sin \theta) \sin \theta
\end{aligned}
$$

- The equations may be rewritten to yield

$$
\begin{aligned}
& \sigma_{x^{\prime}}=\frac{\sigma_{x}+\sigma_{y}}{2}+\frac{\sigma_{x}-\sigma_{y}}{2} \cos 2 \theta+\tau_{x y} \sin 2 \theta \\
& \sigma_{y^{\prime}}=\frac{\sigma_{x}+\sigma_{y}}{2}-\frac{\sigma_{x}-\sigma_{y}}{2} \cos 2 \theta-\tau_{x y} \sin 2 \theta \\
& \tau_{x^{\prime} y^{\prime}}=-\frac{\sigma_{x}-\sigma_{y}}{2} \sin 2 \theta+\tau_{x y} \cos 2 \theta
\end{aligned}
$$

## MECHANIGS OF MATERIALS

Principal Stresses



- The previous equations are combined to yield parametric equations for a circle,

$$
\left(\sigma_{x^{\prime}}-\sigma_{a v e}\right)^{2}+\tau_{x^{\prime} y^{\prime}}^{2}=R^{2}
$$

where

$$
\sigma_{a v e}=\frac{\sigma_{x}+\sigma_{y}}{2} \quad R=\sqrt{\left(\frac{\sigma_{x}-\sigma_{y}}{2}\right)^{2}+\tau_{x y}^{2}}
$$

- Principal stresses occur on the principal planes of stress with zero shearing stresses.

$$
\begin{aligned}
& \sigma_{\max , \min }=\frac{\sigma_{x}+\sigma_{y}}{2} \pm \sqrt{\left(\frac{\sigma_{x}-\sigma_{y}}{2}\right)^{2}+\tau_{x y}^{2}} \\
& \tan 2 \theta_{p}=\frac{2 \tau_{x y}}{\sigma_{x}-\sigma_{y}}
\end{aligned}
$$

Note: definestwoanglesseparatedy $90^{\circ}$

Maximum Shearing Stress



Maximum shearing stress occurs for

$$
\sigma_{x^{\prime}}=\sigma_{a v e}
$$

$$
\begin{aligned}
& \tau_{\max }=R=\sqrt{\left(\frac{\sigma_{x}-\sigma_{y}}{2}\right)^{2}+\tau_{x y}^{2}} \\
& \tan 2 \theta_{s}=-\frac{\sigma_{x}-\sigma_{y}}{2 \tau_{x y}}
\end{aligned}
$$

Note: definestwoanglesseparatedy $90^{\circ}$ and offsetfrom $\theta_{p}$ by $45^{\circ}$

$$
\sigma^{\prime}=\sigma_{a v e}=\frac{\sigma_{x}+\sigma_{y}}{2}
$$

## MECHANIGS OF MATERIALS

## Concept Application 7.1

Fig. 7.13
For the state of plane stress shown, determine (a) the principal planes, (b) the principal stresses, (c) the maximum shearing stress and the corresponding normal stress.

## MECHANICS OF MATERIALS

Concept Application 7.1


## MECHANICS OF MATERIALS

Concept Application 7.1


$$
\begin{aligned}
& \sigma_{x}=+50 \mathrm{MPa} \quad \tau_{x y}=+40 \mathrm{MPa} \\
& \sigma_{x}=-10 \mathrm{MPa}
\end{aligned}
$$

$$
\sigma^{\prime}=20 \mathrm{MPa}
$$



Fig. 7.16

## MECHANICS OF MATERIALS

## Sample Problem 7.1



## SOLUTION:

- Determine an equivalent force-couple system at the center of the transverse section passing through $H$.
- Evaluate the normal and shearing stresses at $H$.
- Determine the principal planes and calculate the principal stresses.

A single horizontal force $P$ of 600 N magnitude is applied to end D of lever $A B D$. Determine (a) the normal and shearing stresses on an element at point $H$ having sides parallel to the $x$ and $y$ axes, (b) the principal planes and principal stresses at the point $H$.

## MECHANICS OF MATERIALS

## Sample Problem 7.1



## SOLUTION:

- Determine an equivalent force-couple system at the center of the transverse section passing through $H$.

$$
\begin{aligned}
P & =600 \mathrm{~N} \\
T & =(600 \mathrm{~N})(0.45 \mathrm{~m})=270 \mathrm{Nm} \\
M_{x} & =(600 \mathrm{~N})(0.25 \mathrm{~m})=150 \mathrm{Nm}
\end{aligned}
$$

- Evaluate the normal and shearing stresses at $H$.

$$
\begin{aligned}
\sigma_{y} & =+\frac{M c}{I}=+\frac{(150 \mathrm{Nm})(0.015 \mathrm{~m})}{\frac{1}{4} \pi(0.015 \mathrm{~m})^{4}} \\
\tau_{x y} & =+\frac{T c}{J}=+\frac{(270 \mathrm{Nm})(0.015 \mathrm{~m})}{\frac{1}{2} \pi(0.015 \mathrm{~m})^{4}}
\end{aligned}
$$

$$
\sigma_{x}=0 \quad \sigma_{y}=+56.6 \mathrm{MPa} \quad \tau_{y}=+50.9 \mathrm{MPa}
$$

## MECHANICS OF MATERIALS

Sample Problem 7.1


## MECHANICS OF MATERIALS

Problems

- 7-19, 7-22


## MECHANICS OF MATERIALS

## Mohr's Circle for Plane Stress



- With the physical significance of Mohr's circle for plane stress established, it may be applied with simple geometric considerations. Critical values are estimated graphically or calculated.
- For a known state of plane stress $\sigma_{x}, \sigma_{y}, \tau_{x y}$ plot the points $X$ and $Y$ and construct the circle centered at $C$.

$$
\sigma_{a v e}=\frac{\sigma_{x}+\sigma_{y}}{2} \quad R=\sqrt{\left(\frac{\sigma_{x}-\sigma_{y}}{2}\right)^{2}+\tau_{x y}^{2}}
$$

- The principal stresses are obtained at $A$ and $B$.

$$
\begin{aligned}
& \sigma_{\max , \min }=\sigma_{a v e} \pm R \\
& \tan 2 \theta_{p}=\frac{2 \tau_{x y}}{\sigma_{x}-\sigma_{y}}
\end{aligned}
$$

The direction of rotation of $O x$ to $O a$ is the same as $C X$ to $C A$.

## MECHANICS OF MATERIALS

## Mohr's Circle for Plane Stress



- With Mohr's circle uniquely defined, the state of stress at other axes orientations may be depicted.
- For the state of stress at an angle $\theta$ with respect to the $x y$ axes, construct a new diameter $X^{\prime} Y^{\prime}$ at an angle $2 \theta$ with respect to $X Y$.
- Normal and shear stresses are obtained from the coordinates $X^{\prime} Y^{\prime}$.


## MECHANIGS OF MATERIALS

## Concept Application 7.2



For the state of plane stress shown, (a) construct Mohr's circle, determine (b) the principal planes, (c) the principal stresses, (d) the maximum shearing stress and the corresponding normal stress.

## MECHANICS OF MATERIALS

Concept Application 7.2
$\tau$ (MPa))


## MECHANICS OF MATERIALS

Concept Application 7.2



- Maximum shear stress

$$
\begin{aligned}
& \theta_{s}=\theta_{p}+45^{\circ} \\
& \theta_{S}=71.6^{\circ}
\end{aligned}
$$

$$
\tau_{\max }=R
$$

$$
\sigma^{\prime}=\sigma_{a v e}
$$

$$
\tau_{\max }=50 \mathrm{MPa}
$$

$$
\sigma^{\prime}=20 \mathrm{MPa}
$$

## MECHANICS OF MATERIALS

## Mohr's Circle for Plane Stress

- Mohr's circle for centric axial loading:

- Mohr's circle for torsional loading:



$$
\sigma_{x}=\sigma_{y}=0 \quad \tau_{x y}=\frac{T c}{J}
$$

$$
\sigma_{x}=\sigma_{y}=\frac{I c}{J} \quad \tau_{x y}=0
$$

## MECHANICS OF MATERIALS

## Sample Problem 7.2



For the state of stress shown, determine (a) the principal planes and the principal stresses, (b) the stress components exerted on the element obtained by rotating the given element counterclockwise through 30 degrees.


SOLUTION:

- Construct Mohr's circle

$$
\begin{aligned}
& \sigma_{a v e}=\frac{\sigma_{x}+\sigma_{y}}{2}=\frac{100+60}{2}=80 \mathrm{MPa} \\
& R=\sqrt{(C F)^{2}+(F X)^{2}}=\sqrt{(20)^{2}+(48)^{2}}=52 \mathrm{MPa}
\end{aligned}
$$

## MECHANIGS OF MATERIALS

## Sample Problem 7.2



- Principal planes and stresses

$$
\begin{array}{rlrl}
\tan 2 \theta_{p} & =\frac{X F}{C F}=\frac{48}{20}=2.4 & \sigma_{\max } & =O A=O C+C A \\
& =80+52 & \sigma_{\max } & =O A=O C-B C \\
2 \theta_{p} & =67.4^{\circ} & & =80-52 \\
\theta_{p} & =33.7^{\circ} \text { clockwise } & \sigma_{\max } & =+132 \mathrm{MPa} \\
& & \sigma_{\min }=+28 \mathrm{MPa}
\end{array}
$$

## MECHANICS OF MATERIALS

## Sample Problem 7.2



- Stress components after rotation by $30^{\circ}$ Points $X^{\prime}$ and $Y^{\prime}$ on Mohr's circle that correspond to stress components on the rotated element are obtained by rotating $X Y$ counterclockwise through $2 \theta=60^{\circ}$


$$
\phi=180^{\circ}-60^{\circ}-67.4^{\circ}=52.6^{\circ}
$$

$$
\sigma_{x^{\prime}}=O K=O C-K C=80-52 \cos 52.6^{\circ}
$$

$$
\sigma_{y^{\prime}}=O L=O C+C L=80+52 \cos 52.6^{\circ}
$$

$$
\tau_{x^{\prime} y^{\prime}}=K X^{\prime}=52 \sin 52.6^{\circ}
$$

$$
\begin{aligned}
& \sigma_{x^{\prime}}=+48.4 \mathrm{MPa} \\
& \sigma_{y^{\prime}}=+111.6 \mathrm{MPa} \\
& \tau_{x^{\prime} y^{\prime}}=41.3 \mathrm{MPa}
\end{aligned}
$$

